Chapter 2: Input Parameters

Overview of Input Preparation

For a quick reference to all TART95 input keywords see the index at the end of this chapter.

Preparing input parameters for a 3-D combinatorial geometry Monte Carlo code can be very complicated, time consuming and frustrating; this is true not only of this code, but of all codes of this type.

It wasn't too long ago that preparing input for a complicated problem and verifying it could take six months to a year; as I said above, it can be very complicated, time consuming and very, very frustrating. Fortunately today with a little planning and using the diagnostic tools that we now have available input preparation can be greatly simplified and sped up and much of the frustration can be avoided.

There are a number of simple steps that you should follow that can greatly simplify input preparation. These include,

- 1) spend time to plan exactly what you want to calculate. In particular, you should have a good drawing or blueprint of your geometry.
- 2) start from a standard, existing input deck and modify it to meet your needs, instead of starting from scratch.
- 3) use **TARTCHEK**, an interactive graphics program, to check your input, before you try using it with TART95.

The most complicated part of input preparation is insuring that the geometry is properly defined. Using **TARTCHEK** can greatly simplify this task for you. There are a number of classic errors that we all occasionally make in input preparation and **TARTCHEK** is designed to allow you to quickly check for these errors.

Somewhat surprisingly, what can also be complicated is properly defining exactly what you want the code to calculate, so that you can properly interpret the output results. For example, if you think the code is calculating influence or path lengths within each zone, when in fact it is actually calculating the leakage crossing zone boundaries, needless to say you will completely misinterpret the results.

TART95 has an enormous number of options to allow you to score almost anything that you want, by zone, position, direction, energy, time, but in order to obtain the results that you actually want you will have to learn what these options are; these will all be described in detail below.

Step by Step Input Preparation

I recommend that you follow the following steps in preparing input parameters.

Step 1: define your geometry. This involves defining a number of spatial zones, where each zone is defined by the surfaces that bound it. Each zone can only be defined by ANDing together all of the bounding surfaces (some Monte Carlo codes allow zones to be defined by AND and OR operations). For example, you can define a zone as being outside a cylinder of radius 5 AND inside a cylinder of radius 10 AND above a plane at -5 AND below a plane at +5 (a cylindrical annulus between two planes). But you cannot define a zone as being below a plane at -5 OR above a plane at +5. This convention will sometimes require that you define more spatial zones than you would like, but in most cases is not too much of an inconvenience.

Every TART95 input deck must define ALL of 3-D space. This isn't as complicated as it sounds at first. The input must define all of the spatial zones that you are really interested in. In addition it must define the rest of ALL space as being outside a non-re-entrant surface that does not contain any material. In this case any particle crossing this non-re-entrant surface can never find its way back into the actual geometry of real interest to you, and the particle can be killed; this is convenient way to terminate histories.

For example, if you have a problem involving ten concentric spheres the input deck must define all space within the ten spheres, but it MUST also define ALL space outside of the sphere of largest radius as a zone containing no material, i.e., a void, in order to allow particle histories to be terminated whenever a particle enters this zone.

Step 2: define all the materials that you will use in your problem. The input to TART95 requires that you define the density (grams/cc) of each material, as well as the composition of each material. The composition of each material can be defined either in terms of the atom fraction of each constituent, e.g., for water 2 atoms of hydrogen and 1 atom of oxygen, or the weight fraction of each constituent. The constituents themselves are in all cases defined by the ZA of the constituent, e.g., ZA = 1001 for hydrogen and 8016 for oxygen.

For all of the materials that you will use in your problem, get all this material together and check it carefully. Are you sure that you have the correct ZA for each constituent, and the correct atom or weight fractions, and correct overall density for each material?

The last step is to assign a number to each material, e.g., material 1, 2, 3, etc. After you have defined all your materials and assigned numbers to each, these material numbers can be used to assign a material to each spatial zone. Remember material number 0 is the definition of a void, and is the default assignment if you do not assign any positive material number. Any particles entering a void will have their histories terminated, so be sure to assign a material to every zone that is not a void. Use **TARTCHEK** to insure that there are no interior void zones.

Defining materials for use with TART95 can often be simplified by using relative density. As we will see below, when a material is assigned to each zone it can be defined in terms of the originally defined material and its overall density multiplied by a relative

density for each zone. If the relative density for a zone is not defined by input, by default it is 1. However, if we have a problem involving exactly the same material, but at different densities in different zones, we need only define one original material and use the relative density for individual zones to properly define the contents of the zone. For example, if we have air at different altitudes and assume that the composition is the same at all altitudes, but its density varies, we can define one standard composition for air and use relative density to define the material at each altitude.

Step 3: define all the physical properties of each zone. Each real, interior zone MUST be assigned a material. In addition for each zone we can define its relative density, as described above, and its temperature if thermal scattering is used.

Whenever a particle enters a zone that does not contain any material its history will be terminated. This applies to the outer most bounding zone, described above, but it also applies to any real interior zone, which mistakenly has not been assigned any material. Every interior zone MUST be assigned a material content. If you want to approximate vacuum in a zone you can make the density of the material extremely small, but you MUST assign something to every real zone. Using this convention puts a burden on the user to insure that every zone does contain a material, but it simplifies TART95's job of tracking particles and more importantly makes it much easier to verify the accuracy of your geometry. Once you feel that your geometry is properly defined you can quickly use TARTCHEK to verify that you have defined all space and that all real interior space contains a material.

Step 4: Decide what type of problem are you going to run. The choices include: static reactivity, dynamic reactivity, or source problems involving incident neutrons, neutron induced photons, incident photons. Decide what is it you want to measure or score as a result.

The type of problem you are going to run will effect some of the input parameters that you should select. What you want to measure will definitely effect your input parameters.

If you are running a source problem write down a complete description of your source or sources: what type of particles are involved (neutrons and/or photons), spatial position, energy spectrum, angular dependence, time dependence. Remember that each problem starts from the source and the results can only be as good as your description of your source. Any error in your source description will propagate throughout your problem.

Minimum Required Input

The minimum input required for any TART95 reactivity or source calculation includes,

- 1) name a name to identify the problem
- 2) box and output ID to direct output (no longer used by TART95)
- 3) surface definitions to define surfaces bounding each zone
- 4) zone definitions to define spatial regions for scoring

- 5) material definitions so that material can be assigned to zones
- 6) assign material to zone required for all zones
- 7) source definition for all problems (reactivity or source)
- 8) end to identify the physical end of input for a problem

Here is an example complete input deck for a fission spectrum of neutrons at the origin in a sphere of water 5 cm in radius,

```
name Red's test
box t32 Red's test
* define a sphere of radius 5 cm
sphere 1 5.0
* zone 1 is inside the sphere
* zone 2 is outside the sphere
              1 1
ib
jb
              2
                 -1
* define water at an overall density of 1 gram/cc
              1 1.0 2 1001 1 8016
* assign water to zone 1 - inside the sphere
               1
matz
* define a point source at the origin
              1 0.0 0.0 0.0
source1
end
```

Everything else, relative density, temperature, weights, what to score, how many histories to run, the energy and angular dependence of the source, etc. all have default values and need not be defined by input. They need not be defined, but it is very important that you understand what all of these defaults are, if you want to be able to properly interpret your results.

For example, if I run the above problem what do I get as output? By default the code will start with a neutron source starting from a point source at the origin (by default it is an isotropic, time independent, fission spectrum). Is this the source that you expected? By default it will track and score both neutrons and neutron induced photons produced, and it will, again by default, score particles entering a zone. The output results for zone 2 (the outside non-re-entrant zone) will be the neutron and photon leakage from the sphere. Since the source starts in zone 1 and no neutrons can leave and re-enter this zone, no neutrons enter the zone and the output will be 0. Is this what you wanted or expected? Would you have properly interpreted the output? In many cases the answer is no. That's why it is important to understand the default values being used, as well as all the scoring options to guarantee that the code runs exactly the problem you want it to run and produces exactly the results that you want.

Allowed Input Parameters

The following sections describe all of the input parameters allowed to be used with TART95. The input parameters used with TART95 are identical to those used with TARTNP, with the exception of a few input options which were judged to be either archaic and out of date or based on experience have demonstrated that they are difficult and dangerous to use. In addition to the input parameters allowed by TARTNP, TART95 includes a few extensions to allow a more general description of input; this is mostly for surface definitions.

Input Lines and Statements

Each input line is free form, blank delimited, with up to 80 characters per line. Input lines can be combined by the use of a continuation indicator (see, Continuation below) to define Input Statements. Each Input Statement starts with a TART95 keyword in the first column, followed by as many input parameters as required to properly define the input option.

Input Fields

Each input line is read as a string of 80 characters (columns 1 through 80), divided into blank delimited field and then each field is interpreted internally.

A blank delimited input field may define text, fixed or floating point numbers. Text can appear at the beginning of an input line to define a TART95 keyword, or it can appear elsewhere to define a filename, or to define a range of input, e.g., the word **thru** is used for this purpose. Fixed, or integer, input fields may start with a sign (+ or -), followed only by integers. Floating point numbers may start with a sign (+ or -) followed by integers, decimal point (optional), and exponent (option), e.g., a floating point 3 may to input as 3.0, 3, 3.0e+0, 0.3e+1, etc.; all are equivalent.

All fixed and floating point fields are internally converted from characters to numbers and how they are used is defined by the expected syntax of each input line, not the actual contents of the input line. For example, an input field of a single digit 3 may be interpreted either to define an integer or floating point number, depending only on the expected syntax of the type of input being read.

Keywords

All keywords are input in lower case; upper case (i.e., capital) characters are not allowed. For example, to define a plane perpendicular to the x axis the keyword **xplane** is acceptable, but XPLANE, or Xplane are not acceptable keywords.

Mandatory versus Optional Input Parameters

Each Input Statement MUST start with a keyword left adjusted to start in the first column of the line. The keyword is followed by as many parameters as are required to properly define the input option. Some parameters are mandatory; for example, in defining a

sphere the user MUST define a positive radius for the sphere. Other parameters may be optional. In describing all keywords mandatory parameters will be listed after the keyword. Any optional parameters will follow the mandatory keywords and will be enclosed in brackets, e.g., [x0 y0].

Comment Lines

Any line that starts with an asterisk (*) in column 1 or c followed by a blank (c) in columns 1 and 2, is a comment line. TART95 input decks may contain any number of comment lines. All comment lines are merely listed in the output report and have no effect on the execution of any problem. Users are encouraged to include comment lines in their input decks in order to completely describe the physical significance of any or all input parameters.

Warning: since some TART95 keywords start with the letter c, c cannot be used to indicate comments, unless it is followed by a blank; only lines starting with an asterisk (*) or c followed by a blank (c) are considered to be comment lines.

Blank Lines

The input deck may contain blank lines anywhere, except before a continuation line. Blank lines MUST be completely blank; not just the first few columns followed by text - they MUST be completely blank.

Continuation

Many input lines may be continued to subsequent lines by including an ampersand (&) as the last character of a line. The first and all continuation lines define an input statement. Continuation lines do not start with a TART95 keyword; they start and continue with input parameters pertinent to the keyword on the first line of the input statement. For example, the following input is correct,

The following input is incorrect, since the second line incorrectly starts with the keyword matz,

Later Input Supersedes Earlier Input

Sometimes you can simplify your input deck by realizing that later input supersedes earlier input. For example if you have a problem with many spatial zones, and most zones contain the same material, and only a few contain a different material, you may be able to

simplify your input deck by realizing that you can first assign the same (most prevalent) material to all of the zones, and later assign a different material to a few zones. For example, the following is legal input,

```
matz 1 1 thru 890
matz 2 17 36 412 671
```

The first line assigns material number 1 to zones 1 through 890, and the second like assigns material 2 to zones 17, 36, 412 and 671, thereby superseding the earlier material assignment to these zones.

You can also use this approach to start from a simple problem for preliminary calculations and add progressively more detail to see what effect it has on results. For example, if you have fuel surrounded by air, surrounded by cladding, surrounded by water, in your preliminary calculation you could assign fuel to the fuel, air and cladding zones, i.e. one **matz** input line. For subsequent calculations you could first add the air and perform a calculation, and then add the cladding and perform another calculation. With this step to step procedure you would be able to simply determine the importance of each change to your system and at each step you need not modify the initial **matz** input line, since you know that any later input will supersede it.

TART95 Extensions

In a number of cases simple extensions have been added to some TARTNP keywords. For example, in the case of cones aligned with a major axis, x, y or x, TARTNP insists that the cone also be centered on the aligned axis, e.g., a cone aligned with the z axis MUST be centered on the z axis. TART95 allows users to specify aligned cones that are not centered on the axis, e.g., for a cone aligned with the z axis, users are allowed to specify x0 and y0 to define the center of the cone. Any TART95 extensions will follow the mandatory keywords and will be enclosed in brackets, e.g., {x0 y0}. Off axis cones cannot be specified as cone input to TARTNP, but they can be specified by the more complicated **surf** input.

Warning: these extensions should ONLY be used with TART95; they have NOT been incorporated in the production version of TARTNP.

Recommended Options

For compatibility with the production version of TARTNP, TART95 uses the same options as TARTNP. However, it is strongly recommended that you use the following options for all neutron problems,

Thermal scattering - define **sentl 39 1** - without turning on thermal scattering, neutrons will continue to slow down to their minimum allowed and end up in a completely unrealistic energy distribution. Even in problems where you think the neutron spectrum will be very fast with no thermal scattering, you have nothing to lose by turning this

option on; if there are no thermal neutrons turning on this option will not result in any penalty in running time, but if there are this is the only way to get realistic results. See, sentl 39, below for an complete description of other parameters to set to correctly use thermal scattering.

Resonance Self-Shielding using the Multi-band Method - define **sentl 20 1** - without turning on the Multi-band method you will be using unshielded multi-group cross sections. The result will be to generally overestimate the mean free path dimensions of systems, and will in most cases give poor results. Turning on this option will increase running time by about 20-30 %, but the improvement in results is generally worth sacrificing the extra running time. Without turning on this option you won't be saving 20-30 % of the running time; you will most likely be wasting 70-80 % of the running time by investing this much time to get unreliable results.

In addition for photon problems (neutron induced photon production and/or independent photon sources) below about 1 MeV, it is recommended that you turn on fluorescence by defining **sentl 25 1**. Failure to turn on fluorescence at lower energies will overestimate photon energy deposition.

From the Beginning to the End

The first line of a problem MUST use the **name** keyword, the second MUST use the **box** keyword and the last line MUST use the **end** keyword.

name problem name

The problem name is up to 40 characters in columns 6 through 45. The first six characters must be unique and should not include special characters such as, +/:, etc. These six characters will be used to define the filename of a restart file. As such, if they are not unique, creation of the restart file may overwrite an existing restart file. Note, presently TART95 does not create restart files, so that this is not currently a problem. However, users should be aware of this convention for compatibility with the production version of TARTNP.

box ann idinfo

Columns 5 through 7 define an output box number and the remaining columns out to column 34 identify the output. In the past **box** was used by the production version of TARTNP to route output files to a computer output box. This is no longer used by TART95 and is included only for compatibility with the existing production version of TARTNP. TART95 leaves all output files on disk at the end of a run and does not attempt to copy them for delivery to a computer output box.

end

Indicates the end of the input for a problem. There are no parameters on this line; it only includes the three characters **end**. An **end** line may be followed by input for another problem; an input deck may contain input for any number of problems. **Warning** - a problem after an **end** line will be read ONLY if the continuation **sentl 24** has been set in the input for the current problem; otherwise the code will terminate at the end of the current problem.

Type of problem - Reactivity or Source

A single keyword **critcalc** defines the type of problem. If this input line is included the problem is a reactivity problem, if this input line is not included the problem is a source problem.

critcalc jsettle nrepeat stat [delt]

A reactivity problem, rather than source problem, will be run. If **delt** is input it will be a dynamic reactivity problem, otherwise a static reactivity problem. **jsettle** is the number of settle cycles to run before starting the calculation; it should be at least 10 to 20 for good results. **nrepeat** is the number of repetitions of the calculation to perform after settling (default =1, only run the calculation once). **stat** is the per-cent standard deviation at which to stop each repetition (default 10.0). **delt** is the time step (shakes) to be used in a dynamic reactivity calculation.

Recommendations: Before running dynamic reactivity calculations it is recommended that you run a static reactivity calculation and then for your dynamic calculation define **delt** to be about one half the removal lifetime found from the static calculation. If you want to insure that the problem runs to convergence insure that **sentl 2** (the maximum number of batches to run) is a large number. The calculation will end when either convergence has been reached (based on the requested standard deviation **stat**) or the maximum number of batches have been run. For quick and dirty results small batches of 500 to 1000 particles per batch (**sentl 3**) are adequate. For very accurate results use more settle cycles (**jsettle**) and larger batches, e.g., 10,000 to 100,000. The total running time to convergence will depend mostly on the total number of histories run (batches times particles per batch), so that except for the overhead during the settle cycles, using larger batches will not greatly increase total running time, e.g., if all other input parameters are the same, using batches of 10,000 instead of 1,000 will not cause the problem to run 10 times as long, because convergence will be reached for a smaller number of batches.

Restrictions: Only neutrons, not photons, are considered during criticality calculations. weight is ignored. Other important input for reactivity calculations include: 1) sentl 2 and 3, that define the maximum number of batches to run and particles per batch - the combination defines the maximum number of histories in a calculation and as such will directly effect running time - for reactivity problems use a very large maximum number of batches if you want to insure that you converge before exceeding the maximum number of batches. Warning - if the maximum number of batches are run before convergence the problem will end and the results will not be reliable, 2) the starting

geometric and energy distribution of the source should be as close as possible to the expected equilibrium distribution. The following input cannot be used for reactivity calculations: ebias, ediscr, maec, maee, maeeh, s9or10e, s11cone, s11cyl, s11dsk, s11sph, sentl 30, source12, source13, source16, source17, timspec

Example Input: To run a dynamic reactivity problem, using 20 settle cycles ($\mathbf{jsettle} = \mathbf{20}$), only perform the calculation once ($\mathbf{nrepeat} = \mathbf{1}$), to within a statistical accuracy of 1 percent ($\mathbf{stat} = \mathbf{1}$), and a time step of .3 shakes (0.003 microseconds) ($\mathbf{delt} = .3$), the following input can be used. By not inputting \mathbf{delta} or setting it to 0, the same input can be used for a static reactivity problem,

critcalc 20 1 1 .3

Geometry

Inside or Outside Surfaces

TART95 uses three dimensional (3-D) combinatorial geometry. The coordinate system is (x, y, z) rectilinear space. Each problem is made up of a number of spatial zones. Each spatial zone is defined by the surfaces that bound the zone. In order to uniquely define zones, in addition to defining which surfaces bound each zone you must also define which side of each surface the zone is located on. For example, if we have a simple problem only involving two concentric spheres, sphere 1 and 2, the problem could involve three spatial zones: 1) inside the inner sphere, 2) between the two spheres, 3) outside the outer sphere. In this case the definition of the three spatial zones should specify that the zones are: 1) inside the inner sphere, 2) outside the inner sphere and **inside** the outer sphere, 3) **outside** the outer sphere. Note, generally it is not sufficient to merely say a surface bounds a zone; you must also specify whether the zone is **inside** or outside the surface. For example, if in the previous example we had said that zone 2) is **inside** both spheres, rather than **outside** the inner sphere and **inside** the outer sphere, we would be describing a different spatial region. You might ask why would one possibly do such a thing. You will find that this is a typical error that one can very easily introduce into problems without realizing it. The concept of **inside** and **outside** surfaces is probably the most difficult thing for users of combinatorial geometry codes to get used to and completely understand; even experienced users will occasionally make errors. Therefore it is worth spending some time discussing it in detail.

TART95 surfaces are either linear or quadratic. Therefore all surfaces can be described by only considering two simply equations,

linear:
$$a(x0 - x) + b(y0 - y) + c(z0 - z)$$

quadratic:
$$r^2 - [a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2]$$

For any given spatial point (x, y, z) and surface with given parameters (x0, y0, z0, a, b, c, r) to determine whether the point is **inside** or **outside** the surface it is sufficient to insert

these parameters into one of the above two equations and solve it. If the answer is **positive** the point is **inside** the surface, if **negative** the point is **outside** the surface, if **zero** the point is **on the surface**. This isn't as complicated as it sounds. Let's consider in detail all of the surfaces that you will have to deal with.

For simple closed surfaces, such as spheres, ellipsoids or cylinders the concept of **inside** and **outside** is fairly intuitive and easy to visualize. If you visualize a sphere, ellipsoid or cylinder you know what **inside** or **outside** means; you are either **inside** or **outside** the object, it's as simple as that. For example, for a sphere the equation is,

$$r^2 - [(x0 - x)^2 + (y0 - y)^2 + (z0 - z)^2]$$

For any spatial point (x, y, z) **inside** the sphere the result of solving this equation is **positive**, for any point **outside** the sphere it is **negative** and for any point **on the surface** of the sphere it is **zero**. So that for these surfaces the concept of **inside** and **outside** is simple to understand.

For open surfaces, such as cones and hyperboloids, it may not be as intuitively obvious what **inside** and **outside** mean. In these cases the surface will be with respect to a reference axis. Any spatial point (x, y, z) that is closer to the reference axis than the surface is **inside** and any point that is further from the axis is **outside**. Think of a cone or hyperboloid as a solid object between the axis and its surface, e.g., for a cone visualize a drinking cup. Can you visualize whether a drop of water is **inside** or **outside** of your drinking cup? If you can, you will have no problem with these surfaces. If not, you can always solve the equation for the surface. For example, for a circular cone aligned with the x axis the equation is,

Pick any (x, y, z) point and solve this equation to define whether or not a point is **inside** or **outside** the surface.

For the last example, consider a plane perpendicular to the x axis at x = x0, the equation of the surface is,

$$x0 - x = 0$$

All spatial points (x, y, z) with x0 > x will be **inside** the surface (since x0 - x > 0), and all points with x0 < x will be **outside** the surface (since x0 - x < 0), and all points with x0 = x will be **on the surface**.

For planes you may prefer to think in terms of **below** and **above** instead of **inside** and **outside**. I encourage you not to do this. For simple aligned planes it may be easy for you

to think of **above** and **below**, but for general rotated planes this can be very confusing. This is also true of general cones. The reason is that in these cases the equations are,

plane:
$$a(x0 - x) + b(y0 - y) + c(z0 - z)$$

cone:
$$-[a (x0 - x)^2 + b (y0 - y)^2 + c (z0 - z)^2], \quad r = 0,$$
two coefficients, a, b, c > 0, one < 0

Note, that by changing the sign of all of the coefficients, a, b, c, we are defining exactly the same surface, but if we solve these equations the meaning of **inside** and **outside** based on the sign of the answer is completely reversed.

Fortunately only in the case of specifying general planes and quadratic surfaces will you be faced by this inconsistency; in all others cases the program will automatically define the sign of all coefficients. Try to remember to define the coefficients a, b, and c, so that **inside** and **outside** make the most sense to you.

If you can understand the concept of **inside** and **outside** for planes, spheres, cylinders, cones, ellipsoids, hyperboloids, you are in, because those are all of the surfaces that you need understand when dealing with TART95. If you don't completely understand the concept don't worry about it; that's the whole purpose of the **TARTCHEK** code, which will completely check your description of geometry and tell you whether or not you have made an error in specifying **inside** or **outside**. If you are not sure of the sign of a surface, rather than worry about it, bang in anything, run **TARTCHEK** and let this interactive graphics program immediately tell you whether or not you have made the right choice.

Preferred axis of orientation

TART95 uses general (x, y, z), 3-D geometry. However, it has a preferred axis of orientation = the z axis; this is strictly for historical reasons. For general 3-D problems there is no advantage to using any preferred axis of orientation. However, for problems that have one or more axii of symmetry there is a definite advantage when using TART95 to defining one axis of symmetry to be the z axis. When this is done: 1) you will be able to use all of the geometry keywords, in particular **surfr**, **surfp** and **srotate**, 2) TART95 can calculate the volume and mass of all zones that are symmetric about the z axis. For general 3-D problems or problems in which you use an axis of symmetry other than the z axis TART95 cannot calculate volumes and mass of zones.

Therefore it is recommended that if your problem has an axis of symmetry, you define this to be the z axis of your geometry. For example, if you have a number of concentric cylinders whose common central axis are all oriented in the same direction, in general it is completely arbitrary what coordinate system you use and what direction you define this central axis to be. However, for use with TART95 it is recommended that you define this to be the z axis. Similarly if you have a number of parallel planes, it is recommended that you define them to be perpendicular to the z axis.

Definition of Surfaces

Surface keywords, Number and Parameters

The definition of each surface starts with a TART95 keyword to define the type of surface, e.g., plane, sphere, cylinder, etc. The keyword is always followed by a surface number; these surface numbers will be used later to define which surfaces bound each spatial zone. The surface number is followed by surface parameters, e.g., the radius of a sphere and position of its center (x0, y0, z0).

First Degree (Planar) Surfaces

All planar surfaces are defined by the first degree equation,

$$dcx (x0 - x) + dcy (y0 - y) + dcz (z0 - z) = 0$$

TART95 allows a general planar surface, plus three special cases of planes aligned with the x, y or z axis. The three special cases correspond to,

```
1) x plane: dcx = 1, dcy = 0, dcz = 0
2) y plane: dcx = 0, dcy = 1, dcz = 0
3) z plane: dcx = 0, dcy = 0, dcz = 1
```

xplane nb x0

a planar surface perpendicular to the x axis at x0. The equation of the surface is,

```
x0 - x = 0

nb - Surface Number x0 - x coordinate of the plane
```

yplane nb y0

a planar surface perpendicular to the y axis at y0. The equation of the surface is,

```
y0 - y = 0

nb - Surface Number
y0 - y coordinate of the plane
```

zplane nb z0

a planar surface perpendicular to the z axis at z0. The equation of the surface is,

$$z0 - z = 0$$

nb - Surface Number

z0 - z coordinate of the plane

a general plane passing through the point (x, y, z) = (x0, y0, z0), with the vector normal to the surface (dcx, dcy, dcz). (dcx, dcy, dcz) are optional input parameters; if not specified they default to (0, 0, 1), which corresponds to a zplane. The equation of the surface is,

$$dcx (x0 - x) + dcy (y0 - y) + dcz (z0 - z) = 0$$

nb - Surface Number

x0 - x coordinate of the plane

y0 - y coordinate of the plane

z0 - z coordinate of the plane

dcx - direction cosine to x axis

dcy - direction cosine to y axis

dcz - direction cosine to z axis

Second Degree (Quadratic) Surfaces

All second degree surfaces are defined by the equation,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

TART95 allows a general second degree surface, plus special cases for spheres and ellipsoids, as well as for circular cylinders and cones that are aligned with the x, y or z axis. TART95 also allows second degree surfaces to be translated and rotated after their initial definition.

Spheres

The equation of all spheres is,

$$(x0 - x)^2 + (y0 - y)^2 + (z0 - z)^2 = r^2$$

Direct Definition of Spheres

The input for the following keywords differ only in the order that the x0, y0, and z0 coordinates are input. In all cases the input defines a sphere of radius r centered at the point (x, y, z) = (x0, y0, z0).

spherex nb r [x0 z0 y0]

spherey nb r [y0 z0 x0]

nb - Surface Number

r - Radius of the sphere

x0 - x center of sphere

y0 - y center of sphere

z0 - z center of sphere

Restrictions: the radius (r) must be positive. x0, y0, z0 are optional input and default to 0, 0, 0 (the origin of your coordinate system), if not input.

"Two Point" Spheres

A sphere centered on the x, y or z axis may be defined in terms of two points that it passes through. In order to uniquely define a sphere the two points must be different. In each case the program will solve two simultaneous equations to define the radius and center of the sphere. For example, in the case of a sphere centered on the x axis (y0 = z0) = 0, the equation of the surface is,

$$(x0 - x)^2 + y^2 + z^2 = r^2$$

The sphere passes through the two points (r, x) = (r1, x1) and (r2, x2), where r is the radius from the x axis. The program solves,

$$(x0 - x)^2 = r^2 - (y^2 + z^2)$$

$$(x0 - x1)^2 = r1^2$$

$$(x0 - x2)^2 = r2^2$$

to define r and x0.

These two point spheres can be very useful if you want to guarantee that combinations of surfaces meet exactly at any given set of points.

The following keywords differ only in terms of which of the three axes the sphere is centered on, x, y or z.

spher2px nb r1 x1 r2 x2

a sphere centered on the x axis, (y0 = z0 = 0), and passing through the two points (r, x) = (r1, x1) and (r2, x2), where r is the radius from the x axis. The equation of the surface is,

$$(x0 - x)^2 + y^2 + z^2 = r^2$$

The program will solve to define r and x0.

nb - Surface Number

r1, x1- Point the sphere passes through

r2, x2- Point the sphere passes through

Restriction: x1 and x2 must differ.

a sphere centered on the y axis (x0 = z0 = 0), and passing through the two points (r, y) = (r1, y1) and (r2, y2), where r is the radius from the y axis. The equation of the surface is,

$$x^2 + (y^0 - y)^2 + z^2 = r^2$$

The program will solve to define r and y0.

nb - Surface Number

r1, y1- Point the sphere passes through

r2, y2- Point the sphere passes through

Restriction: y1 and y2 must differ.

a sphere centered on the z axis (x0 = y0 = 0), and passing through the two points (r, z) = (r1, z1) and (r2, z2), where r is the radius from the z axis. The equation of the surface is,

$$x^2 + y^2 + (z_0 - z)^2 = r^2$$

The program will solve to define r and z0.

nb - Surface Number

r1, z1 - Point the sphere passes through

r2, z2- Point the sphere passes through

Restriction: z1 and z2 must differ.

Ellipsoids

The equation of all ellipsoids is,

$$[(x0 - x)/sx]^2 + [(y0 - y)/sy]^2 + [(z0 - z)/sz]^2 = 1$$

an ellipsoid centered at the point (x, y, z) = (x0, y0, z0), with semi-axis sx, sy and sz parallel to the x, y and z axes, respectively.

or, in the standard form described above,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

 $a = 1/sx^2$

 $b = 1/sy^2$

 $c = 1/sz^2$

r = 1

An Ellipsoid may be defined directly or if symmetric about the z axis, in terms of two points that it passes through.

ellipse nb sx sy sz [z0 x0 y0]

an ellipsoid centered at the point (x, y, z) = (x0, y0, z0), with semi-axis sx, sy and sz parallel to the x, y and z axes, respectively.

nb - Surface Number

sx - x semi-axis

sy - y semi-axis

sz - z semi-axis

z0 - z center of ellipsoid

x0 - x center of ellipsoid

y0 - y center of ellipsoid

Restrictions: all of the semi-axis, sx, sy, sz, must be positive. z0, x0, y0, are optional input and default to 0, 0, 0, if not input.

ellip2p nb z0 r1 z1 r2 z2

an ellipsoid centered at z = z0, symmetric around the z axis, (x0 = y0 = 0), and passing through the two points (r, z) = (r1, z1) and (r2, z2), where r is the radius from the z axis. The equation of the surface is,

$$x^2 + y^2 + c (z_0 - z)^2 = r^2$$

The program will solve two simultaneous equations to define the radius, r, and c.

nb - Surface Number

r1, z1- Point the ellipsoid passes through

r2, z2- Point the ellipsoid passes through

Restrictions: z1 and z2 must differ and the point further from z0 must have the smaller r coordinate.

Circular Cylinders

TART95 allows three special cases of circular cylinders, where the axis of the cylinder is aligned with one of the three major axes, x, y or z. In these cases the equation of circular cylinders is,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

where two of the coefficients, a, b and c, are positive and equal, the third is zero and r is positive.

For elliptic and/or non-aligned cylinders see **surfr**, **surfp**, and **srotate**, below.

a right circular cylinder of radius r, parallel to the x axis, whose axis passes through the point (x, y, z) = (0.0, y0, z0). The equation of the surface is,

$$(y0 - y)^2 + (z0 - z)^2 = r^2$$

nb - Surface Number

z0 - z center of cylinder

y0 - y center of cylinder

Restrictions: r must be positive. z0, y0, are optional input and default to 0, 0, if not input.

cyly
$$nb r [z0 x0]$$

a right circular cylinder of radius r, parallel to the y axis, whose axis passes through the point (x, y, z) = (x0, 0.0, z0). The equation of the surface is,

$$(x0 - x)^2 + (z0 - z)^2 = r^2$$

nb - Surface Number

z0 - z center of cylinder

x0 - x center of cylinder

Restrictions: r must be positive. z0, x0, are optional input and default to 0, 0, if not input.

cylz nb r x0 y0

cyl nb r x0 y0

a right circular cylinder of radius r, parallel to the z axis, whose axis passes through the point (x, y, z) = (x0, y0, 0.0). The equation of the surface is,

$$(x0 - x)^2 + (y0 - y)^2 = r^2$$

nb - Surface Number x0 - x center of cylinder y0 - y center of cylinder

Restrictions: r must be positive. x0, y0, are optional input and default to 0, 0, if not input.

Circular Cones

TART95 allows three special cases of circular cones, where the axis of the cone is aligned with one of the three major axes, x, y or z. In these cases the equation of circular cones is,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

where two of the coefficients, a, b and c, are positive and equal, the third is negative and r is zero.

For elliptic and/or non-aligned cones see **surfr**, **surfp**, and **srotate**, below.

Direct Definition of Circular Cones

conex nb ang [x0] {y0 z0} xcone nb ang [x0] {y0 z0}

a right circular cone, symmetric around the x axis, with its vertex at x = x0, and making an angle ang (degrees) with the x axis. The equation of the surface is,

$$a (x0 - x)^2 - (y0 - y)^2 - (z0 - z)^2 = 0$$

nb - Surface Number

ang - angle (degrees) between x axis and surface of cone

x0 - x vertex of cone y0 - y vertex of cone z0 - z vertex of cone

Restrictions: the angle ang may not be 0 or 90 degrees. x0 is optional input that defaults to 0 if not input. y0 and z0 are TART95 extensions that cannot be used with the TARTNP program.

coney nb ang [y0] $\{x0 \ z0\}$

ycone nb ang
$$[y0]$$
 $\{x0 \ z0\}$

a right circular cone, symmetric around the y axis, with its vertex at y = y0, and making an angle ang (degrees) with the y axis. The equation of the surface is,

$$-(x0-x)^2 + b(y0-y)^2 - (z0-z)^2 = 0$$

nb - Surface Number

ang - angle (degrees) between y axis and surface of cone

y0 - y vertex of cone x0 - x vertex of cone z0 - z vertex of cone

Restrictions: the angle ang may not be 0 or 90 degrees. y0 is optional input that defaults to 0 if not input. x0 and z0 are TART95 extensions that cannot be used with the TARTNP program.

```
conez nb ang [z0] {x0 y0}
zcone nb ang [z0] {x0 y0}
cone nb ang [z0] {x0 y0}
```

a right circular cone, symmetric around the z axis, with its vertex at z = z0, and making an angle ang (degrees) with the z axis. The equation of the surface is,

$$-(x0-x)^2 - (y0-y)^2 + c(z0-z)^2 = 0$$

nb - Surface Number

ang - angle (degrees) between z axis and surface of cone

z0 - z vertex of cone x0 - x vertex of cone z0 - z vertex of cone

Restrictions: the angle ang may not be 0 or 90 degrees. z0 is optional input that defaults to 0 if not input. x0 and y0 are TART95 extensions that cannot be used with the TARTNP program.

"One Point" Circular Cones

Circular cones aligned with one of the major axis, x, y, or z, may also be defined by defining the vertex of the cone and one point that the cone passes through.

conerx nb x0 r1 x1

a right circular cone, symmetric around the x axis, with its vertex at x = x0, and passing through the point (r, x) = (r1, x1), where r is the radius from the x axis. The equation of the surface is.

$$a(x0 - x)^2 - y^2 - z^2 = r^2$$

The program will solve for a.

nb - Surface Number

x0 - x vertex of cone

r1,x1 - a point the cone passes through

Restrictions: x0 and x1 must differ.

conery nb y0 r1 y1

a right circular cone, symmetric around the y axis, with its vertex at y = y0, and passing through the point (r, y) = (r1, y1), where r is the radius from the y axis. The equation of the surface is,

$$-x^2 + b(y^0 - y)^2 - z^2 = 0$$

The program will solve for b.

nb - Surface Number

y0 - y vertex of cone

r1,y1 - a point the cone passes through

Restrictions: y0 and y1 must differ.

conerz nb z0 r1 z1 coner nb z0 r1 z1

a right circular cone, symmetric around the z axis, with its vertex at z = z0, and passing through the point (r, z) = (r1, z1), where r is the radius from the z axis. The equation of the surface is,

$$-x^2 - y^2 + c(z^0 - z)^2 = 0$$

The program will solve for c.

nb - Surface Number

z0 - z vertex of cone

r1,z1 - a point the cone passes through

Restrictions: z0 and z1 must differ.

"Two Point" Circular Cones

Circular cones aligned with one of the major axis, x, y, or z, may also be defined by defining two points that the cone passes through.

cone2px nb r1 x1 r2 x2

a right circular cone, symmetric around the x axis, and passing through the two points (r, x) = (r1, x1) and (r2, x2), where r is the radius from he x axis. The equation of the surface is,

$$a(x0 - x)^2 - y^2 - z^2 = r^2$$

The program will solve for a and x0.

nb - Surface Number

r1,x1 - a point the cone passes through

r2,x2 - a point the cone passes through

Restrictions: x1 and x2 must differ.

cone2py nb r1 y1 r2 y2

a right circular cone, symmetric around the y axis, and passing through the two points (r, y) = (r1, y1) and (r2, y2), where r is the radius from the y axis. The equation of the surface is,

$$-x^2 + b(y0 - y)^2 - z^2 = 0$$

The program will solve for b and y0.

nb - Surface Number

r1,y1 - a point the cone passes through

r2,y2 - a point the cone passes through

Restrictions: y1 and y2 must differ.

a right circular cone, symmetric around the z axis, and passing through the two points (r, z) = (r1, z1) and (r2, z2), where r is the radius from the z axis. The equation of the surface is,

$$-x^2 - y^2 + c(z^0 - z)^2 = 0$$

The program will solve for c and z0.

nb - Surface Number

r1,z1 - a point the cone passes through

r2,z2 - a point the cone passes through

Restrictions: z1 and z2 must differ.

General Aligned Quadratic Surfaces

A general aligned quadratic surface is defined by the equation,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

There are seven types of real quadratic surfaces possible with this equation. For example, for a quadratic aligned with the z axis and a and b in standard form, positive, the seven types are as follows,

- 1) Sphere a = b = c, r > 0
- 2) Circular Cylinder a = b, c = 0, r > 0
- 3) Circular Cone a = b, c < 0, r = 0
- 4) Ellipsoid c > 0, r > 0

The above four can be defined using the above keywords. The following three can be defined using **surf** and **surfr** keywords.

- 5) Elliptic Cylinder c = 0, r > 0
- 6) Elliptic Cone c < 0, r = 0
- 7) Hyperboloid of one sheet c < 0, r > 0

For non-aligned quadratics **surfr** can be used to define an aligned quadratic that can subsequently be translated and/or rotated using **surfp** or **srotate**, see below.

surf nb r c [z0 x0 y0 a b]

a quadratic surface centered at (x, y, z) = (x0, y0, z0), defined by the equation,

$$a(x0-x)^2 + b(y0-y)^2 + c(z0-z)^2 = r^2$$

nb - Surface Number

r - constant, e.g., a radius

c - coefficient for z term

z0 - z center

x0 - x center

y0 - y center

a - coefficient for x term

b - coefficient for y term

Restrictions: z0, x0, y0, are optional input that default to 0, 0, 0, if not input a and b are optional input that default a = b = 1.0, in which case the surface is symmetric about the z axis.

surfr nb r c [a b]

a quadratic surface centered at the origin, and symmetric around the z axis, defined by the equation,

$$a x^2 + b y^2 + c z^2 = r^2$$

Note, this is identical to **surf** with x0 = y0 = z0 = 0.

nb - Surface Number
r - constant, e.g., a radius
c - coefficient for z term
a - coefficient for x term
b - coefficient for y term

Restrictions: a and b are optional input that default a = b = 1.0, in which case the surface is symmetric about the z axis.

Any surface that is defined using **surfr** may be subsequently translated and rotated using **surfp** and **srotate**, to define non-aligned quadratics.

Translation and Rotation

Surfaces previously defined by **surfr** input may be subsequently translated and rotated. Note, for a collection of objects that all have the same center, as defined by **surfr** input, the following keywords may be used to translate and rotate the entire collection of objects, e.g., define a simply aligned object at the origin and subsequently translate and rotate the entire object. The following keywords are used to translate and rotate surfaces,

surfp nb x0 y0 z0 [dex dey dez]

nb must be a surface previously described by **surfr** input. The center of symmetry, initially at the origin, is translated to the point (x, y, z) = (x0, y0, z0). The axis of the surface, initially the +z axis, is rotated to the direction (dcx, dcy, dcz).

nb - Surface Number

x0 - x center y0 - y center z0 - z center

dcx - direction cosine to x axis

dcydirection cosine to y axisdczdirection cosine to z axis

Restrictions: surface number nb must have been previously defined by **surfr** input. (dcx, dcy, dcz) are optional input that default to (dcx, dcy, dcz) = (0, 0, 1), which corresponds to no rotation; this option can be used to translate surfaces, without rotation.

srotate nb nb1 nb2 nb3.....

nb must be a surface previously described by **surfr** input, and assigned a translation and rotation by a **surfp** input. **nb1**, **nb2**, **nb3**....must also have been previously described by **surfr** input. The surfaces **nb1**, **nb2**, **nb3**...will be assigned the same translation and rotation as that assigned to **nb**.

This keyword is a convenient means of assigning the same translation and rotation to a collection of surfaces. The same thing can be accomplished by inputting **surfp** lines all with the same translation and rotation parameters for each of the surfaces **nb**, **nb1**, **nb2**, **nb3**.......

nb - A previously defined **surfr** surface number
nb1 - A previously defined **surfr** surface number
nb2 - "

Restrictions: surface number nb must have been previously defined by both **surfr** and **surfp** input lines. Surface numbers **nb1**, **nb2**,... must have been previously defined by **surfr** input.

Definition of Zones

Each spatial zone is defined by the surfaces that bound the zone. In order to uniquely define zones, in addition to defining which surfaces bound each zone you must also define which side of each surface the zone is located on.

TART95 uses three different types of zones: 1) normal real interior zones that you are interested in; these MUST contain material, 2) an exterior non-re-entrant zone (the rest of the universe); this MUST not contain material, and 3) reflecting zones; these MUST not contain material. The first two types of zones are defined using **jb** and **zonejb** or **bjp** keywords; these are described immediately below. Reflecting zones will be defined after describing **jb**, **zonejb** and **bjp**.

Interior and Exterior Zones

Each problem may use one of two possible ways to define zones: you can either use **jb** or **bjp** input, but you cannot mix the two together in a single problem. With **jb** input you define each of the bounding surfaces and a sign to say whether the zone is inside or

outside of the surface. With **bjp** input for each bounding surface you define the same information as with **jb** input, plus you define the most probable zone that a particle will enter if it leaves the current zone across this surface. With **jb** input the code will learn as it progresses through a problem what zone a particle will enter if it leaves the current zone across this surface and optimize the zone search strategy accordingly. With **bjp** input the code will always assume that the new zone entered will be exactly the one indicated by input and it will not attempt any further optimization. The **recommended** option is to use **jb** input; **bjp** input should only be used in special cases, as will be explained in detail below.

nz is a zone number (1 to MAXZONE) and **nb1**, **nb2**, **nb3**,....are signed surface numbers. Blank or plus as the first character of **nb1**, **nb2**, etc., indicates that the zone is **inside** the surface, **minus** indicates the zone is **outside** the surface.

For example, if I have two spherical surfaces of different radii and three zones: 1) **inside** the inner sphere, 2) **outside** the inner sphere and **inside** the outer sphere, 3) **outside** the outer sphere, the definition of the three zones could be,

```
* Definition of 2 spherical surfaces
```

```
sphere 1 5.0 sphere 2 8.0
```

* Definition of 3 zones by their bounding surfaces

jb 1 1 jb 2 -1 2 ib 3 -2

This first defines surfaces 1 and 2 as spheres of radius 5 and 8 cm, respectively, centered on the origin (default x0, y0, z0 = 0, 0, 0). It next defines zone 1 to be inside the sphere of radius 5, zone 2 to be outside the sphere of radius 5 and inside the sphere of radius 8, and zone 3 to be outside the sphere of radius 8.

The input line may be continued to any number of successive lines by ending a line with an ampersand (&). Continuation lines do not include the keyword, jb or zonejb, or the zone number nb; they only contain signed surface numbers. For example, if zone 1 is bounded by surfaces 6 through 18 (with various signs) the input could look like the following,

If the zone were bounded by more surfaces additional continuation lines can be used (as many as are required to define all bounding surfaces).

Restrictions: this option cannot be used when **bjp** input is used, see below. All of the surface numbers used as boundaries of each zone must all be defined by input.

bjp nz nb1 mp1 nb2 mp2 nb3 mp3......[&]

This is an infrequently used option to describe zones, and is only used for special applications, usually involving overlapped geometry, as explained in detail below.

Restrictions: this option cannot be used when **jp** input is used, see below. All of the surface numbers used as boundaries of each zone, and all most probable zones must be defined by input.

nz is a zone number (1 to MAXZONE), **nb1**, **nb2**, **nb3**,....are positive surface numbers and **mp1**, **mp2**, **mp3**,....are signed most probable zone numbers that the particle will enter when it crosses surfaces **nb1**, **nb2**, **nb3**..., respectively. Blank or plus indicated that the zone is **inside** the surface, **minus** indicates the zone is **outside** the surface.

For example, if I have two spherical surfaces of different radii and three zones, two of which overlap: 1) **inside** the inner sphere, 2) **inside** the outer sphere, 3) **outside** the outer sphere, the definition of the three zones could be,

* Definition of 2 spherical surfaces

sphere 1 5.0 sphere 2 8.0

* Definition of 3 zones by their bounding surfaces

bjp 1 1 2 bjp 2 2 3 bjp 3 2 -2

In order to understand how this input is interpreted the user has to understand how TART95 searches for zones. When a particle leaves one zone the code determines which zone it has entered by searching the list of zones and using the bounding surfaces to determine if the current (x, y, z) space point is in a given zone. The list of zones is searched in a circular fashion starting at the most probable zone, if necessary continuing to the maximum zone number defined in the problem, and if necessary continuing from the first zone up to the most probable zone (the entire list of zones is searched in a circular fashion).

Assume that we have a source of particles at the origin of the concentric spheres and we wish to determine the leakage of particles from each sphere. If we wish to determine the leakage from a number of spheres of different radii we could use **jb** or **zonejb** and run separate calculations for each radius. However, using **bjp** input we can obtain the answers we want in one single calculation.

The trick to use in doing this is to have overlapping zones, where zones of smaller radius are totally contained within zones of larger radius, and zones of smaller radius have

smaller zone numbers, and the most probable zone always indicates a zone with a larger radius, with the except of the last, outer most zone; presumably a vacuum non-re-entry zone, where merely for completeness the most probable zone may be defined as the zone just inside it. Lastly it is important when defining the source to indicate that its most probable zone is the inner most zone.

For the above description of zones and a source at the origin all source particles will initially be in zone 1. They will transport until they disappear or cross the first spherical surface and leave zone 1. At this point the search for the zone that has been entered will start at the most probable zone number when leaving zone 1 and crossing surface 1 = zone 2, as indicated by the above input. In this case the search will always indicate that the particle has entered zone 2 (since in this simple example it is the only zone immediately outside of the first spherical surface). Again particles will transport in zone 2 until they disappear or leave the zone. But note that in this case, since the only bounding surface for zone 2 is surface 2, the outer spherical surface, the particle can never re-enter zone 1; if it crosses the inner spherical surface traveling inward or outward, based on the defined bounding surfaces of zone 2, it remains in zone 2. If the particle does leave zone 2 by crossing the outer spherical surface the search for the next zone will begin at the most probable zone when leaving zone 2 and crossing surface 2 = zone 3, as indicated by the above input. In this case the search will always indicate that the particle has entered zone 3 (since this is the only zone immediately outside the outer spherical surface), and the history will be terminated, assuming that this outer most zone 3 is a vacuum, non-reentry zone.

So what are our results? If we are scoring what enters each zone, what enters zone 2 is the leakage from a sphere with the inner radius, and what enters zone 3 is the leakage from a sphere with the outer radius. In other words, in one calculation we have calculated the leakage from both spheres.

This is a trivial example, but hopefully the reader can understand that if we had defined ten, twenty, or any number of concentric spheres, the leakage from all of them could be calculated in only one calculation.

Using **bjp** input has a number of advantages and disadvantages.

The advantages include: 1) potentially large savings in computer time if you can calculate many results in a single problem, 2) the results are guaranteed to be statistically correlated, since in the same run you are using exactly the same histories, e.g., if you perform a number of separate calculations due to statistics you may end up with the non-physical conclusion that the leakage across some larger radius spheres is more than that across some smaller radius spheres.

The disadvantages include: 1) this input can be very complicated and it is very easy to make errors and incorrectly define the input, 2) with overlapping geometry it is not possible to use the input checking codes, such as **TARTCHEK**, to help verify the accuracy of your input, 3) there aren't that many real problems where it is possible to

completely overlap geometry, as we have done in the simple example problem used above, 4) the savings in computer time isn't as large as one might think; the overall running will be dominated by the largest zone defined.

Based on experience I do not recommend that you use this option. It has been included in TART95 only for completeness, since it is a TARTNP option. For any real problem involving complicated geometry it is simply far too easy to make mistakes in the input geometry description, that can lead to disastrous results. In my opinion it is better to be conservative and use **jb** or **zonejb** input with non-overlapping geometry. You can then use the available interactive graphics program **TARTCHEK** to quickly verify your description of geometry and then run TART95. Alternatively, if you do decide to use **bjp** and overlapping geometry, you are on your own as far as verifying the accuracy of your description of geometry = caveat emptor.

Reflecting Zones

Using reflecting zones can in some cases greatly simplify input preparation. By taking advantage of any symmetries in a problem you may be able to only model a smaller portion of a problem and use reflection to simulate the entire problem, thus simplifying your input deck and minimizing the amount of work you have to do to prepare the deck. For example, you can simulate an infinitely repeating pattern of planes using only one repetition of the pattern and reflecting boundaries.

TART95 ALWAYS uses 3-D geometry. Even if you have a 1-D series of planes or an infinite cylinder you MUST close your geometry to define 3-D space finite volume space. For an infinite cylinder you can use two reflecting planes orthogonal to the axis of the cylinder to close your geometry. For a series of planes you can use four reflecting planes orthogonal to your planes to close your geometry.

Be careful when defining reflecting zones to insure that the results really exactly simulate your true geometry; it is very easy to make logic mistakes and end up with a problem description that does not correspond to the geometry you are trying to model. For example, in the case of a series of planes, rather than using four orthogonal planes to close your geometry you might think it is easy and equivalent to use a single reflecting cylinder orthogonal to your planes; this is not equivalent. You can stack an infinite array of cubes to exactly fill your 3-D space by using four reflecting planes and reflection from these planes will exactly simulate what would have happened had a particle actually crossed a plane and entered an adjacent cell. In contrast, you cannot stack a series of cylinders to exactly fill your 3-D space and reflection from the cylindrical surface will not exactly simulate what would have happened had a particle actually crossed the cylinder and entered an adjacent cell.

Warning - when using reflecting boundaries you will obtain the same results as if you had modeled the entire system; this is true only integrated over each zone, but not per unit volume or mass. Remember that the volumes calculated by this code will only be for the real interior zones of your problem, and particles can only transport in these real

zones. Therefore per incident source particle calculated total path lengths, etc. will be exactly the same as in a problem where you model the entire system. However, per unit volume the results for these zones will be larger than the result you would obtain not using reflecting zones and modeling the entire system. The results will be larger exactly in proportion of the ratio of the volume of a zone in the entire system to that in your system with reflectors. For example, if you have a cylindrically symmetric system and you use a reflecting plane on its axis to only model one half of the system, the calculated total path length, etc. will be the same as if you had modeled the entire system. But since the volume of your system with a reflector is only half that of the entire system your results per unit volume or mass will be twice as large as it would have been had you modeled the entire system without a reflector. You MUST consider this effect in order to properly interpret the output results.

TART95 uses specula reflection to reflect neutrons and photons off a boundary when a zone is identified as a reflecting zone. Note, input identifies zones, not surfaces, as reflecting; particles are reflected off of any bounding surface of a zone that is identified as a reflecting zone. For reflection the code calculates the normal to the surface that the particle crossed entering the reflecting zone and derives the direction cosines such that the incident particle, the surface normal, and the reflected particle are coplanar.

For historical reasons TART95 allows a number of keywords to define that a zone is a reflector. These keywords seem to refer to different types of surfaces, rather than to zones. As actually used in the code all are equivalent; any zone that is identified as reflecting will always reflect particles, regardless of the types of surfaces that bound it, e.g., planes, spheres, cylinders, etc.. The only except is that the code will print the number of particles that have reflected off of **xplane**, **yplane** or **zplane**. If this information is of interest to you, you should use the appropriate reflection keyword. Otherwise use any of the following keywords interchangeably.

reflx nz1 nz2 nz3...

Zones nz1, nz2, nz3...are reflecting zones. These zones need only one **xplane** boundary. These zones are assigned material -1, to identify them as x reflectors.

refly nz1 nz2 nz3...

Zones nz1, nz2, nz3...are reflecting zones. These zones need only one **yplane** boundary. These zones are assigned material -2, to identify them as y reflectors.

reflz nz1 nz2 nz3...

Zones nz1, nz2, nz3...are reflecting zones. These zones need only one **zplane** boundary. These zones are assigned material -3, to identify them as z reflectors.

reflgp nz1 nz2 nz3...

Zones nz1, nz2, nz3...are reflecting zones. These zones need only one **genplane** or **gpl** boundary. These zones are assigned material -5, to identify them as general plane reflectors.

reflq nz1 nz2 nz3...

Zones nz1, nz2, nz3...are reflecting zones. These zones need only one quadratic boundary. These zones are assigned material -4, to identify them as quadratic reflectors.

As mentioned above, zones, not surfaces, reflect, so that any of these keywords may be used interchangeable for input. Regardless of what type of surface a particle crosses when entering a zone, the particle will be correctly reflected based on the type of surface crossed, e.g., plane, sphere, cylinder, etc., regardless of the keyword used on input to define the zone as reflecting. For example, even if you identify a reflecting zone using the keyword **reflx** if the particle crosses a spherical surface to enter the zone it will be correctly reflected from a **sphere**, not a **xplane**.

Restrictions: Reflecting zones MUST not have a material assigned to them. If you assign material to a reflecting zone you can overwrite the assigned negative material numbers, - 1 through -5, which is used to define a zone as reflecting (as described above), in which case the zone will no longer be a reflector.

Material Definitions

Each material is defined by specifying its overall density in grams/cc and each one of its constituents. Constituents are defined by specifying either their atomic or weight fraction and the ZA (1000*Z+A) of the isotope or element. Two TART95 keywords are defined to allow specification by either atomic or weight fraction,

matl m rho f(1) za(1) f(2) za(2)......[&]

m - assigned material number

rho - material overall density in grams/cc

f(1) - atom fraction of the first constituent

za(1) - ZA of the first constituent

f(2) - atom fraction of the second constituent

za(2) - ZA of the second constituent

For example, water has two atoms of hydrogen (ZA=1001) to each atom of oxygen (ZA=8016). For water at an overall density of 1.0 grams/cc the input would be,

matl 1 1.0 2.0 1001 1.0 8016

Note, the 1 following matl defines this as material number 1.

Restrictions: The overall density MUST be positive. Different material numbers should be assigned to each material. The atom fractions need not be normalized to the actual atoms/cc; these are merely relative atom fractions. Each problem may use up to 50 different materials. Each material may contain up to 25 different constituents. **matl** and **matlwp** input may both be used in the same problem.

matlwp m rho f(1) za(1) f(2) za(2)......[&]

m - assigned material number

rho - material overall density in grams/ccf(1) - weight fraction of the first constituent

za(1) - ZA of the first constituent

f(2) - weight fraction of the second constituent

za(2) - ZA of the second constituent

For example, concrete at an overall density of 2.32 grams/cc, with 5% Al rebar and impurities of Ti, Sc and Ni, the input would be,

```
matlwp 2 2.32 .005683 1001 .502588 8016 .026720 11023 & .017647 12000 .091026 13027 .255033 14000 .062213 20000 & .0001 24000 .035493 26000 .000199 29000 .000199 30000 & .001 28000
```

Note, the use of continuation lines, indicated by & as the last character of an input line. Note, the 2 following matl defines this as material number 2.

Restrictions: The overall density MUST be positive. Different material numbers should be assigned to each material. The weight fractions need not be normalized to the actual grams/cc; these are merely relative weight fractions. Each problem may use up to 50 different materials. Each material may contain up to 25 different constituents. **matlwp** and **matl** input may both be used in the same problem.

Zonal Properties

You can define the following zonal properties for each zone individually or for all zones; if you do not define the zonal properties by input you will be using the default value indicated in parenthesis,

- 1) material number assigned to zone (0)
- 2) minimum neutron energy or zone temperature (2.53e-08 MeV)
- 3) minimum photon energy (-1.0e-04 MeV)
- 4) relative density (1.0)
- 5) neutron weight, used for splitting (1.0)
- 6) photon weight, used for splitting (1.0)

- 7) photon production multiplier (1.0)
- 8) neutron edit (output results) type (3)
- 9) photon edit (output results) type (3)
- 10) request additional edits (output results) (0)

Zonal properties are defines in one of two forms,

keyword value nz1 thru nz2

or

keyword value nz1 nz2 nz3.....

These forms cannot be combined on one input line. However, a combination of the two may be used. In any problem latter input lines supersede earlier input lines, so that the most widely used value can first be assigned to all zones and later input lines can change the value for specific zones. For example, if zone 20 has a weight of 1.0, zones 8, 10 and 12 a weight of 2.0, and all remaining zones a weight of 4.0, the following input can be used.

```
weight 4.0 1 thru 30 weight 2.0 8 10 12 weight 1.0 20
```

```
matz m nz1 nz2 nz3....(0)
matz m nz1 thru nz2
```

Material number **m** is assigned to the indicated zones, **nz1**, **nz2**, **nz3**... or **nz1** through **nz2**. Note, the default (0) in the above example indicates that if you do not explicitly answer a material number, **m**, to a zone, by default material number 0 (void; a terminus zone) is assigned to the zone.

Restrictions: Material number **m** must be defined by **matl** or **matlwp** input. A material number MUST be assigned to all interior zones, A material MUST NOT be assigned to exterior, non-re-retrant zones or reflecting zones.

```
TART99 Update volume nz1 vz1 nz2 vz2 nz3 vz3.....
```

The volume (in cc) for zones **nz1**, **nz2**, **nz3**... is defined by input to be **vz1**, **vz2**, **vz3**..., respectively. TART will attempt to analytically calculate the volume of each zone. When it cannot analytically calculate the volume you can use the input option **mcvdisk or mcvplane** to statistically sample the volume. In order to accurately statistically sample volumes can be very time consuming. This input option allows you to statistically sample volumes only once, and then in all following calculations you need merely define them

by input. This will allow you to correctly define volumes that can effect special output, such as deposition in MeV/cc or MeV/grams, see **probm** and **sentl 35.**

Example Input: The following input line defines the volume of zones 2 17 and 23 to be 1.34, 13.7 and 213.6 cc, respectively,

```
Volume 2 1.34 17 13.7 23 213.6
```

Restrictions: The zone numbers **nz1**, **nz2**, **nz3**... MUST be 1 to the maximum number of zones used in the problem, and all volumes be **vz1**, **vz2**, **vz3**... MUST be positive. The volumes that you input are used by TART without questioning their accuracy, and no attempt is made to analytically calculate the volumes of these zones.

```
emin e nz1 nz2 nz3....(2.53e-08)
emin e nz1 thru nz2 (2.53e-08)
```

emin has two different meanings depending on whether or not thermal scattering is being used (**sentl 39**). If thermal scattering is not being used **emin** defines the minimum neutron energy in each zone. If thermal scattering is being used **emin** defines the temperature of zones in MeV; in this case only **sentl 8** can be used to define the minimum neutron energy.

When thermal scattering is not being used **emin** and **sent1 8** control the minimum allowed neutron energy (MeV) in each zone. **emin** can be used to define the minimum energy zone by zone; **sent1 8** allows it to be defined globally as the same value for all zones.

When thermal scattering is not being used, the absolute value of \mathbf{e} is the minimum allowed energy (MeV) of neutrons in these zones. For photons use **eming**. After a collision if a neutron's energy is less than the absolute value of \mathbf{e} : 1) if \mathbf{e} is positive the neutron's energy is set equal to \mathbf{e} , 2) if \mathbf{e} is negative the neutron history is terminated.

Recommendations: When thermal scattering is used the following options should also be used: **sentl 8 1.307e-09**, otherwise the code will use the default 2.53e-08 and the neutrons will not be able to completely thermalize and, **sentl 13 1.307e-09**, otherwise the code will use the default and not tally neutrons below 2.53e-08 entering zones with tally type 11 and 12.

Restrictions: the default minimum energy and temperature for all zones is 2.53e-08 (room temperature). The minimum neutron energy MUST be within the limits of the multigroup neutron energy range: 1.307e-09 to 20 MeV. The temperature of a zone must be positive.

```
eming e nz1 nz2 nz3....(-1.0e-04)
eming e nz1 thru nz2 (-1.0e-04)
```

eming and **sentl 9** control the minimum allowed photon energy (MeV) in each zone. **emin** can be used to define the minimum energy zone by zone; **sentl 9** allows it to be defined globally as the same value for all zones.

The absolute value of \mathbf{e} is the minimum allowed energy (MeV) of photons in these zones. For neutrons use **emin**. After a collision if a photon's energy is less than the absolute value of \mathbf{e} : 1) if \mathbf{e} is positive the photon's energy is set equal to \mathbf{e} , 2) if \mathbf{e} is negative the photon history is terminated.

Restrictions: the default minimum energy for all zones is -1.0e-04, i.e., terminate any photon history if the photon energy is less than 100 eV. The minimum photon energy MUST be within the limits of the photon data range: 1.0e-04 to 30 MeV.

eta r nz1 nz2 nz3.....(1.0)

The relative density \mathbf{r} is assigned to the indicated zones. The overall density of a zone, in grams/cc, is defined as the product of the density of the material assigned to the zone times the relative density.

Restrictions: The default value is 1.0. Relative density must be positive.

```
weight w nz1 nz2 nz3.... (1.0) weight w nz1 thru nz2 (1.0)
```

w is the neutron statistical weight for zone nz1, nz2, nz3...or nz1 through nz2, and the photon statistical weight if wgtgam input is not used. Weights other than 1.0 can be used in high attenuation problems to force particle flow into spatial regions of interest. At a zone boundary crossing, the product of weight and number of particles is conserved. For example, if a particle crosses from a high weight zone into a low weight zone, the particle is split. If a particle crosses from a low weight zone into a high weight zone, particles are statistically discarded.

Recommendations: **Warning** - Use zonal weights with extreme care. Do not try to drastically change weights over relatively small distances (small in terms of mean free paths). Be absolutely sure that the ratio of weights in adjacent zones is 1/2, 1 or 2; this is often difficult to do in complicated geometries, where one zone may be adjacent to many other zones.

As a rough guideline in using weights, remember that a source will be exponentially attenuated according to the total mean free path. About every 0.7 mean free paths a source will be attenuated by a factor of 2. Therefore if you 1/2 the weight every 0.7 mean free path the number of source particles will remain approximately constant. If you want this to happen you can run a very short calculation (see **sentl 2** and **3** to minimize the number of histories) and reading the output report to determine the mean free path of the materials that you are using at your source energy. This will tell you how to zone your problem to allow you to use weights to propagate a source deep into a medium.

Restrictions: The default weight for all zones is 1.0. Weights are ignored in criticality (static or dynamic) calculations. ALL weights MUST be powers of 2, e.g., 1, 2, 4, 8,...1/2, 1/4, 1/8, etc. The ratio of weights in adjacent zones MUST be 1/2, 1 or 2, i.e., large changes in weights between adjacent zones are not allowed - the weight can change by at most a factor of 2. In going from a high to low weight zone the particle is split into exactly two particles, and in going from a low to high weight zone one half the particles are discarded - **Warning** - this procedure is correct only if the ratio of weights in adjacent zones is 1/2, 1 or 2.

```
wgtgam w nz1 nz2 nz3.... (1.0)
wgtgam w nz1 thru nz2 (1.0)
```

w is the photon statistical weight for zones nz1, nz2, nz3...or nz1 through nz2. Weights other than 1.0 can be used in high attenuation problems to force particle flow into spatial regions of interest. At a zone boundary crossing, the product of weight and number of particles is conserved. For example, if a particle crosses from a high weight zone into a low weight zone, the particle is split. If a particle crosses from a low weight zone into a high weight zone, particles are statistically discarded.

Recommendations: **Warning** - Use zonal weights with extreme care. Do not try to drastically change weights over relatively small distances (small in terms of mean free paths). Be absolutely sure that the ratio of weights in adjacent zones is 1/2, 1 or 2; this is often difficult to do in complicated geometries, where one zone may be adjacent to many other zones.

As a rough guideline in using weights, remember that a source will be exponentially attenuated according to the total mean free path. About every 0.7 mean free paths a source will be attenuated by a factor of 2. Therefore if you 1/2 the weight every 0.7 mean free path the number of source particles will remain approximately constant. If you want this to happen you can run a very short calculation (see **sentl 2** and **3** to minimize the number of histories) and reading the output report to determine the mean free path of the materials that you are using at your source energy. This will tell you how to zone your problem to allow you to use weights to propagate a source deep into a medium.

Restrictions: The default weight for all zones is 1.0. **weight** input lines change the default if **wgtgam** input is not used. ALL weights MUST be powers of 2, e.g., 1, 2, 4, 8,...1/2, 1/4, 1/8, etc. The ratio of weights in adjacent zones MUST be 1/2, 1 or 2, i.e., large changes in weights between adjacent zones are not allowed - the weight can change by at most a factor of 2. In going from a high to low weight zone the particle is split into exactly two particles, and in going from a low to high weight zone one half the particles are discarded - **Warning** - this procedure is correct only if the ratio of weights in adjacent zones is 1/2, 1 or 2.

```
gpwgt w nz1 nz2 nz3.... (1.0)
gpwgt w nz1 thru nz2 (1.0)
```

Photon (gamma ray) production multiplier. w multiplies the number of photon produced per neutron collision. The resulting photons are tracked and scored with weight 1/w.

Recommendations: photon multipliers can be used to good advantage in combination with neutron (weight) and photon (wgtgam) statistical weights to minimize variance and speed convergence, particularly in thick media that strongly attenuate photons, e.g., almost any high atomic number (Z) material. In this case without using photon multipliers you may not generate enough photons deep enough in the material to obtain statistically reliable results.

Restrictions: The default is 1.0, i.e., track and score exactly the number of photons produced per neutron collision. The multiplier MUST be positive. **Warning** - you CANNOT use this option to try and turn off photon production and tracking in zones by using a multiplier of zero, since photons are assigned a weight of 1/w.

For zone by zone output tally options for neutrons (type) and photons (typeg), as well as notal, units and zonemult see Neutron and Photon Edit and Tally (Output) types, later in this report.

Sources

Every problem MUST include a source; this includes reactivity calculations, as well as neutron and/or photon source problems.

In order to uniquely define a source distribution you MUST define the source: 1) type of particle (neutrons and/or photons), 2) energy spectrum, 3) angular distribution, 4) time distribution, and 5) spatial distribution. All source parameters have default values.

Type of Particle

sentl 1 defines the type of source particles and what particles to track. The default value is **sentl 1 0**, neutron source particles, track neutrons and neutron induced photon production. **sentl 1** can be used to define other types of sources, see **sentl 1**, below.

Energy Distribution

Neutron spectrum

The default is a neutron induced fission spectrum of neutrons. For monoenergetic sources the energy can be defined using **sentl 4** For an actual spectrum there are many options, that are described below.

Photon spectrum

The default is a neutron induced fission spectrum of photons. For monoenergetic sources the energy can be defined using **sentl 17**. For an actual spectrum there are many options, that are described below.

Neutrons Photons Distribution

4 sentinel to define monoenergetic source 34 sentinel for fission spectrum temperature

ediscr ediscrg a series of monoenergetic sources s9or10e s9or10eg energy dependent spectrum

espec especg energy dependent spectrumfspec fspecg energy dependent spectrum

ehist ehistg histogram energy dependent spectrumeangl eanglg correlated angle-energy distribution

enerangl enranglg correlated angle-energy distribution

maee maeeg correlated angle-energy distribution

maeeh maeehg correlated angle-energy distributionmaec maecg correlated angle-energy-time distribution

blkbdy blackbody photon source spectrum

ebias ebiasg bias energy distribution

Each of these is described in detail below.

blkbdy [temp emax thin]

The photon source will be a blackbody spectrum with a temperature of **temp** extending up to a maximum energy of **emax**, with a maximum fractional deviation of **thin** from an exact blackbody spectrum.

Restrictions: **temp, emax** and **thin** are optional input that default to **temp** = 0.001 MeV, **emax** = 15.0***temp** and **thin** = 0.003. If input **temp, emax** and **thin** MUST all be positive.

ebias j
$$w(j)$$
 $e(j)$ $w(j+1)$ $e(j+1)$

The neutron source spectrum is biased by assigning weights using the piece wise linear distribution defined by the weights $\mathbf{w}(\mathbf{j})$ and energies $\mathbf{e}(\mathbf{j})$.

Restrictions: The minimum and maximum energies MUST correspond EXACTLY to those of the input spectrum. The number of neutrons sampled at each energy will be determined by the sampling weight, and the relative weight of each sampled neutron will be equal to the ratio of the actual spectrum to the weighted spectrum.

ebiasg j
$$w(j)$$
 $e(j)$ $w(j+1)$ $e(j+1)$

The photon source spectrum is biased by assigning weights using the piece wise linear distribution defined by the weights $\mathbf{w}(\mathbf{j})$ and energies $\mathbf{e}(\mathbf{j})$.

Restrictions: The minimum and maximum energies MUST correspond EXACTLY to those of the input spectrum. The number of photons sampled at each energy will be

determined by the sampling weight, and the relative weight of each sampled photon will be equal to the ratio of the actual spectrum to the weighted spectrum.

ediscr fn1 e1 fn2 e2.....

The neutron source spectrum will have discrete energies, with the relative number of neutrons fn1, fn2.... at the discrete energies e1, e2,......

Restrictions: Do not use for reactivity problems. Any number of **ediscr** input lines may be used. All **ediscr** input lines are combined to define the final relative number of neutrons at each discrete energy.

ediscrg fn1 e1 fn2 e2.....

The photon source spectrum will have discrete energies, with the relative number of photons **fn1**, **fn2**.... at the discrete energies **e1**, **e2**,......

Restrictions: Any number of **ediscrg** input lines may be used. All **ediscrg** input lines are combined to define the final relative number of photons at each discrete energy.

ehist j rn(j) e(j) rn(j+1) e(j+1)...... 0.0 emax

The neutron source spectrum is a histogram distribution defined by the relative number of neutrons per unit energy $\mathbf{rn}(\mathbf{j})$ in the energy interval $\mathbf{e}(\mathbf{j})$ to $\mathbf{e}(\mathbf{j}+1)$.

Restrictions: Any number of **ehist** input lines may be used to define the complete spectrum. The final **rn** MUST be 0.0 at the maximum energy **emax**. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: The following input defines a histogram spectrum between 6.7743 and 15.242 MeV.

```
      ehist
      1 0.01433 6.7743 0.01010 7.5479 0.007873 8.3633

      ehist
      4 0.004204 9.2205 0.006741 10.120 0.002353 11.060

      ehist
      7 0.003448 11.547 0.003121 12.043 0.00434 12.550

      ehist
      10 0.02450 13.068 0.02234 13.863 0.02609 14.134

      ehist
      13 0.01429 14.407 0.0 15.242
```

ehistg j rn(j) e(j) rn(j+1) e(j+1)...... 0.0 emax

The photon source spectrum is a histogram distribution defined by the relative number of photons per unit energy $\mathbf{rn}(\mathbf{j})$ in the energy interval $\mathbf{e}(\mathbf{j})$ to $\mathbf{e}(\mathbf{j}+1)$.

Restrictions: Any number of **ehistg** input lines may be used to define the complete spectrum. The final **rn** MUST be 0.0 at the maximum energy **emax**. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: See, ehist, above for example input.

eangl and **eanglg** are used to define the angular distribution of neutron and photon sources, and are used in conjunction with **enerangl** and **enranglg** to define a completely correlated angle-energy distribution. For a description of **eangl** and **eanglg** see **ANGULAR DISTRIBUTIONS**.

enerangl
$$j$$
 $e(j)$ $c(j)$ $e(j+1)$ $c(j+1)$

The neutron source spectrum is a completely correlated angle-energy distribution. **eangl** defines the angular distribution and is first sampled to define a cosine. **enerangl** defines the completely correlated energy, in terms of a piece wise linearly interpolable table of energies, $\mathbf{e}(\mathbf{j})$, corresponding to any sampled cosine $\mathbf{c}(\mathbf{j})$.

Restrictions: The tabulated cosine range defined by the **enerangl** c(j) input MUST span at least the same range as the cosine range defined by **eangl** input.

enranglg
$$j$$
 $e(j)$ $c(j)$ $e(j+1)$ $c(j+1)$

The photon source spectrum is a completely correlated angle-energy distribution. **eanglg** defines the angular distribution and is first sampled to define a cosine. **enranglg** defines the completely correlated energy, in terms of a piece wise linearly interpolable table of energies, $\mathbf{e}(\mathbf{j})$, corresponding to any sampled cosine $\mathbf{c}(\mathbf{j})$.

Restrictions: The tabulated cosine range defined by the **enranglg** c(j) input MUST span at least the same range as the cosine range defined by **eanglg** input.

espec
$$j$$
 rn(j) e(j) rn($j+1$) e($j+1$).....

The neutron source spectrum is a piecewise linearly interpolable defined by the relative number of neutrons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **espec** input lines may be used to define the entire spectrum. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: The following input defines a piecewise linear spectrum between 6.7743 and 15.242 MeV. Note, the below spectrum is similar to the spectrum defined above for **ehist**, however here when we use the keyword **espec** the spectrum is interpreted as piecewise linear, whereas in the case of **ehist** it is interpreted as histograms,

```
espec 1 0.01433 6.7743 0.01010 7.5479 0.007873 8.3633 espec 4 0.004204 9.2205 0.006741 10.120 0.002353 11.060
```

espec 7 0.003448 11.547 0.003121 12.043 0.00434 12.550

espec 10 0.02450 13.068 0.02234 13.863 0.02609 14.134

espec 13 0.01429 14.407 0.0 15.242

especg j rn(j) e(j) rn(j+1) e(j+1).....

The photon source spectrum is a piecewise linearly interpolable defined by the relative number of photons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **especg** input lines may be used to define the entire spectrum. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: See, **espec**, above for example input.

fspec
$$j$$
 $f(j)$ $e(j)$ $f(j+1)$ $e(j+1)$

The neutron source spectrum is a piecewise linearly interpolable defined by the relative number of neutrons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$, where $\mathbf{rn}(\mathbf{j}) = \mathbf{f}(\mathbf{j})/\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **fspec** input lines may be used to define the entire spectrum. All energies $\mathbf{e}(\mathbf{j})$ MUST be positive; otherwise in attempting to define $\mathbf{rn}(\mathbf{j}) = \mathbf{f}(\mathbf{j})/\mathbf{e}(\mathbf{j})$ there will be an obvious problem. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: The following input defines a piecewise linear spectrum between 6.7743 and 15.242 MeV. Note, the below spectrum is similar to the spectrum defined above for **ehist**, and **espec**, however here when we use the keyword **fspec** the spectrum is interpreted as piece wise linear, but with a variation that is different from the **espec** interpretation, since here the relative number of neutrons is $\mathbf{rn}(\mathbf{j}) = \mathbf{f}(\mathbf{j})/\mathbf{e}(\mathbf{j})$,

```
fspec 1 0.01433 6.7743 0.01010 7.5479 0.007873 8.3633 fspec 4 0.004204 9.2205 0.006741 10.120 0.002353 11.060 fspec 7 0.003448 11.547 0.003121 12.043 0.00434 12.550 fspec 10 0.02450 13.068 0.02234 13.863 0.02609 14.134 fspec 13 0.01429 14.407 0.0 15.242
```

fspecg j f(j) e(j) f(j+1) e(j+1).....

The photon source spectrum is a piecewise linearly interpolable defined by the relative number of photons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$, where $\mathbf{rn}(\mathbf{j}) = \mathbf{f}(\mathbf{j})/\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **fspecg** input lines may be used to define the entire spectrum. All energies $\mathbf{e}(\mathbf{j})$ MUST be positive; otherwise in attempting to define $\mathbf{rn}(\mathbf{j}) = \mathbf{f}(\mathbf{j})/\mathbf{e}(\mathbf{j})$ there will be an obvious problem. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: See, **fspec**, above for example input.

For a description of **maec** and **maecg**, that are used by define angular and time distributions to be used in conjunction with **maee**, **maeeh**, **maeeg** and **maeehg**, to define correlated angle-energy-time distributions, see **Angular Distributions**.

maee i j rn(j) e(j) rn(j+1) e(j+1).....

Neutron source energy spectrum i is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maee** input and the energy distribution is defined by **maee** input. The neutron source spectrum is a piecewise linearly interpolable defined by the relative number of neutrons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Do not use for reactivity problems. Any number of **maee** input lines may be used to define the entire spectrum. The energies $\mathbf{e}(\mathbf{j})$ MUST be monotonically increasing or decreasing. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: The following input uses **maec** and **maee** input to define two different spectra: the first for the cosine range 1.0 to 0.9, and the second for the cosine range 0.9 to 0.866. Note, the **maec** input defines the angular ranges (with a default launch time = 0) and the **maee** input defines the spectrum in each cosine range. Note, since **maee** is used the input is interpreted as piece wise linearly interpolable, in contrast to **maeeh** input which is interpreted as histogram.

```
* Neutron source for cosine = 1.0 to 0.9
maec 1
          167
               1.0 0.9
maee 1
            1
                3.08e-07 3.316e-02 9.26e-07 6.74e-02
            3
maee 1
                5.86e-06 9.6e-02
                                   2.56e-05 0.135
maee 1
                8.27e-05 0.318
                                   2.4e0-4 0.75
                2.19e-04 2.02
maee 1
* Neutron source for cosine = 0.9 to 0.866
                0.9 0.866
maec 2
          753
maee 2
            1
                6.17e-07 4.73e-02 4.6e-06
                                            7.8e-02
maee 2
            3
                1.04e-07
                          0.1
                                   1.99e-04 0.18
maee 2
            5
                 6.2e-04
                          0.42
                                   1.01e-03 1.0
maee 2
            7
                 5.6e-04
                          2.8
```

maeeg i j rn(j) e(j) rn(j+1) e(j+1).....

Photon source energy spectrum \mathbf{i} is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maeeg** input and the energy distribution is defined by **maeeg** input. The neutron source spectrum is a piecewise linearly interpolable defined by the relative number of photons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **maeeg** input lines may be used to define the entire spectrum. The energies e(j) MUST be monotonically increasing or decreasing. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example input: see above under **maee**.

```
maeehi j rn(j) e(j) rn(j+1) e(j+1)....0.0 emax
```

Neutron source energy spectrum i is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maec** input and the energy distribution is defined by **maech** input. The neutron source spectrum is a histogram distribution defined by the relative number of neutrons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Do not use for reactivity problems. Any number of **maee** input lines may be used to define the entire spectrum. The energies $\mathbf{e}(\mathbf{j})$ MUST be monotonically increasing or decreasing. The final \mathbf{rn} MUST be 0.0 at the maximum energy \mathbf{emax} . The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example Input: The following input uses **maec** and **maeeh** input to define two different spectra: the first for the cosine range 1.0 to 0.9, and the second for the cosine range 0.9 to 0.866. Note, the **maec** input defines the angular ranges (with a default launch time = 0) and the **maeeh** input defines the spectrum in each cosine range. Note, since **maeeh** is used the input is interpreted as a histogram distribution, in contrast to **maee** input which is interpreted as piece wise linearly.

```
* Neutron source for cosine = 1.0 to 0.9
maec 1
          167
               1.0 0.9
maeeh 1
                3.08e-07 3.316e-02 9.26e-07 6.74e-02
            1
maeeh 1
                5.86e-06 9.6e-02
                                   2.56e-05 0.135
maeeh 1
            5
                                   2.4e0-4 0.75
                8.27e-05 0.318
maeeh 1
                0.0
                         2.02
* Neutron source for cosine = 0.9 to 0.866
maec 2
          753
                0.9 0.866
maeeh 2
            1
                6.17e-07 4.73e-02 4.6e-06
                                             7.8e-02
maeeh 2
            3
                1.04e-07 0.1
                                    1.99e-04 0.18
maeeh 2
            5
                 6.2e-04
                           0.42
                                    1.01e-03 1.0
maeeh 2
                 0.0
                           2.8
```

i j rn(j) e(j) rn(j+1) e(j+1)....0.0 emax

maeehg

Photon source energy spectrum \mathbf{i} is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maeeg** input and the energy distribution is defined by **maeehg** input. The neutron source spectrum is a histogram distribution defined by the relative number of photons per unit energy $\mathbf{rn}(\mathbf{j})$ at each energy $\mathbf{e}(\mathbf{j})$.

Restrictions: Any number of **maeehg** input lines may be used to define the entire spectrum. The energies **rn(j)** MUST be monotonically increasing or decreasing. The final **rn** MUST be 0.0 at the maximum energy **emax**. The code integrates the entire spectrum to define 1000 equally probable sampling bins.

Example input: see above under **maeeh**.

For a neutron shell source defined the **i-th source9** or **source10** input line, the initial source energy distribution will be sampled from a number of discrete energies, where $\mathbf{rn}(\mathbf{j})$ is the relative number of neutrons at discrete energies $\mathbf{e}(\mathbf{j})$.

Restrictions: All energies MUST be within the range of the neutron data, 1.3o7e-09 to 20 MeV. Do not use with reactivity problems.

s9or10eg i j
$$rn(j)$$
 e(j) $rn(j+1)$ e(j+1)......

For a photon shell source defined the **i-th s9g** or s10g input line, the initial source energy distribution will be sampled from a number of discrete energies, where rn(j) is the relative number of photons at discrete energies e(j).

Restrictions: All energies MUST be within the range of the photon data, 1.0e-04 to 30 MeV.

Angular Distribution

Neutron Angular Distribution

The default is an isotropic angular distribution. The angular distribution can be defined using **sentl 6** and **7**, or using one of the options described below.

Photon Angular Distribution

The default is an isotropic angular distribution. The angular distribution can be defined using **sentl 41** and **42**, or using one of the options described below.

Neutrons	Photons	Distribution		
anglsrce	anglsrg	define angular range		
6, 7	41, 42	sentinels to define angular range		
axis	axisg	switch source orientation		
eangl eanglg	correlate	ed angle-energy distribution		
enerangl	enrangl	g correlated angle-energy distribution		
maee maeeg correlated angle-energy distribution				
maeeh maeeh	g (correlated angle-energy distribution		
maec maecg	correlate	ed angle-energy-time distribution		

anglsrce a1 a2

The neutron source angular distribution will be uniform between the angles **a1** and **a2** (degrees) from the reference axis, which by default is the positive z axis.

Restrictions: Only one **anglsrce** input can be used in a problem. **anglsrce** is an alternative to **sentl 6** and **7** input to define the neutron source angular distribution. The reference axis can be changed using **sentl 32**, **axis**, **source3**, **source4** or **source6**.

anglsrg a1 a2

The photon source angular distribution will be uniform between the angles **a1** and **a2** (degrees) from the reference axis, which by default is the positive z axis.

Restrictions: Only one **anglsrg** input can be used in a problem. **anglsrce** is an alternative to **sentl 41** and **42** input to define the neutron source angular distribution. The reference axis can be changed using **sentl 45**, **axisg**, **s3g**, **s4g** or **s6g**.

The neutron source reference axis for launching source3, source4 or source9 is the directed line between the two points (x1, y1, z1) and (x2, y2, z2).

Restrictions: (x1, y1, z1) and (x2, y2, z2) MUST be two distinct points. sentl 30 (switch reference axis) is ignored. The angular distribution about the reference axis may be defined using anglsrce or sentl 6 and 7.

The photon source reference axis for launching s3g, s4g or s9g is the directed line between the two points (x1, y1, z1) and (x2, y2, z2).

Restrictions: (x1, y1, z1) and (x2, y2, z2) MUST be two distinct points. sentl 32 (switch reference axis) is ignored. The angular distribution about the reference axis may be defined using anglsrg or sentl 41 and 42.

eangl j
$$rn(j)$$
 $c(j)$ $rn(j+1)$ $c(j+1)$

The neutron source angular distribution will be sampled from the piecewise linear distribution defined by the relative number of neutrons $\mathbf{rn}(\mathbf{j})$ and the cosines $\mathbf{c}(\mathbf{j})$. The neutron energy will then be defined by interpolation in the table of energy versus direction cosine define by **enerangl** input.

Restrictions: The reference axis for the cosines c(j) is the x axis. When either is used both eangl and enerangl MUST be defined by input.

eanglg j
$$rn(j)$$
 $c(j)$ $rn(j+1)$ $c(j+1)...$

The photon source angular distribution will be sampled from the piecewise linear distribution defined by the relative number of neutrons $\mathbf{rn}(\mathbf{j})$ and the cosines $\mathbf{c}(\mathbf{j})$. The

photon energy will then be defined by interpolation in the table of energy versus direction cosine define by **enranglg** input.

Restrictions: The reference axis for the cosines c(j) is the z axis. When either is used both eanglg and enranglg MUST be defined by input.

maec i w c1 c2 [t1 t2]

Neutron source energy spectrum **i** is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maec** input and the energy distribution is defined by **maee** or **maeeh** input. For **maec** input the relative number of neutrons to launch for source spectrum **i** is defined by weight **w**. The neutrons are launched in a uniform distribution between the cosines **c1** and **c2** and between times **t1** and **t2**.

Restrictions: Do not use for reactivity problems. **t1** and **t2** are optional input that default to 0, 0. Any number of **maec** input lines may be used to completely define the neutron source distribution. The source number **i** is used in both **maec** and **maee** or **maeeh** input to define which input to correlate. The reference axis is the z axis, unless specified by a **source6** input line, or **source13** input (which uses the normal to a spherical surface).

For a description of **maee** and **maeeh** input to use with **maee** input to define a correlated angle-energy-time neutron source distribution, see **Energy Distribution**.

maecg i w c1 c2 [t1 t2]

Photon source energy spectrum **i** is a correlated angle-energy-time distribution. The angular-time distribution is defined by **maecg** input and the energy distribution is defined by **maeeg** or **maeehg** input. For **maecg** input the relative number of photons to launch for source spectrum **i** is defined by weight **w**. The photons are launched in a uniform distribution between the cosines **c1** and **c2** and between times **t1** and **t2**.

Restrictions: **t1** and **t2** are optional input that default to 0, 0. Any number of **maecg** input lines may be used to completely define the photon source distribution. The source number **i** is used in both **maecg** and **maeeg** or **maeehg** input to define which input to correlate. The reference axis is the z axis, unless specified by a **s6g** input line, or **s13g** input (which uses the normal to a spherical surface).

For a description of **maeeg** and **maeehg** input to use with **maeeg** input to define a correlated angle-energy-time photon source distribution, see **Energy Distribution**.

Time Distribution

Neutron Time distribution

The default is time independent or initial starting time = 0. The initial time for neutron sources can be defined using **sentl 31**. For an actual time distribution use one of the options described below.

Photon Time distribution

The default is time independent or initial starting time = 0. The initial time for photon sources can be defined using **sentl 44**. For an actual time distribution use one of the options described below.

Neutrons Photons Distribution

31 44 sentinels to define initial time

timdisttimdistgtime distributiontimspectimspecgtime distribution

maec maecg correlated angle-energy-time distribution

For a description of **maec** and **maecg**, that are used by define angular and time distributions to be used in conjunction with **maee**, **maeeh**, **maeeg** and **maeehg**, to define correlated angle-energy-time distributions, see **Angular Distribution**. For a description of **maee**, **maeeh**, **maeeg** and **maeehg**, see **Energy Distribution**.

timdist
$$j$$
 $t(j)$ $t(j+1)$ $t(j+2)$

The neutron source's time coordinate will be sampled from the equally probability time intervals t(j), t(j+1), t(j+2)....(shakes), with uniform sampling in each time interval.

Restrictions: Do not use in reactivity problems. The times $\mathbf{t}(\mathbf{j})$ must be positive and in increasing input order. At least one pair of times $\mathbf{t}(\mathbf{j})$, $\mathbf{t}(\mathbf{j+1})$ MUST be defined to allow sampling over some time interval.

timdistg
$$j$$
 $t(j)$ $t(j+1)$ $t(j+2)$

The photon source's time coordinate will be sampled from the equally probability time intervals t(j), t(j+1), t(j+2)....(shakes), with uniform sampling in each time interval.

Restrictions: The times t(j) must be positive and in increasing input order. At least one pair of times t(j), t(j+1) MUST be defined to allow sampling over some time interval.

timspec
$$j$$
 $m(j)$ $t(j)$ $rn(j+1)$ $t(j+1)$

The neutron source's time coordinate will be sampled from the continuous, piecewise linear spectrum defined by the relative number of particles $\mathbf{rn}(\mathbf{j})$ at each time $\mathbf{t}(\mathbf{j})$.

Restrictions: Do not use in reactivity problems. At least one pair of times t(j), t(j+1) MUST be defined to allow sampling over some time interval.

timspecg
$$j rn(j) t(j) rn(j+1) t(j+1)...$$

The photon source's time coordinate will be sampled from the continuous, piecewise linear spectrum defined by the relative number of particles $\mathbf{rn}(\mathbf{j})$ at each time $\mathbf{t}(\mathbf{j})$.

Restrictions: At least one pair of times t(j), t(j+1) MUST be defined to allow sampling over some time interval.

Spatial Distribution

The default spatial distribution is a point source at the origin of the coordinate system. The options are,

Neutrons	Photon	s Distribution
source1	s1g	a point source
source2	s2g	cylindrical shell source
source3	s3g	spherical shell source
source4	s4g	spherical surface source
source5	s5g	rectangular parallelepiped source
source6	s6g	directed point source
source9	s9g	multiple spherical shell sources
s9		"
source10	s10g	multiple cylindrical shell sources
s10		"
s11cone	s11cor	neg multiple conical surface sources
s11cyl s11cylg		multiple cylindrical surface sources
s11dsks11dskg		multiple annulus of disk sources
s11sph s11sphg		multiple spherical surface sources
source12	s12g	general source read from a file
s12iso		isotropic general source read from a file
source13	s13g	segment of a spherical surface source
source15	s15g	segment of a cylindrical surface source
s15		"
source16	s16g	arc of a spherical surface source
source17	s17g	directed spherical surface source
32	45	sentinels to switch source axii

Each source spatial distribution includes: 1) a TART95 keyword defining the type of source, 2) the most probable zone that the source is in, 3) the parameters defining the source coordinates.

The most probable zone is used to optimize the search for the starting zone of each source particle. In many cases the entire spatial source distribution will be in a single zone, in which case it is easy to define the most probable zone. In other cases the distribution may be in a number of zones, in which case you can define the most probable zone as the zone where most of the source particle will originate. In complicated geometries with complicated source distributions it may not be possible for you to decide what is the most probable zone. In this case, don't worry about it. Remember specifying the most probable zone is used merely to optimize the search for the starting zone. If you are not sure what

zone this is, just guess, and specify any reasonable zone number that is being used in your problem. The worst a bad guess can do is cause the code to run for a slightly longer time.

The restriction on all sources is that they be within the real interior zones. They cannot lie outside the geometry, nor should point sources be on the boundary of one or more zones. If you have a defined geometry and want to see the effect of particles incident on your geometry you can either: 1) define an additional zone containing air and adjacent to your geometry, so that you can start your source in this zone, or, 2) start you source very close to, but inside the surface of a zone, e.g., for a source incident on a series of planes, start the source 1.0e-06 cm inside the plane closest to the source.

A neutron point source at (x0, y0, z0). The most probable zone that the source is located in is nz.

Restrictions: $\mathbf{x0}$, $\mathbf{y0}$, $\mathbf{z0}$ are optional input that default to 0, 0, 0 (the origin) if not input. The point ($\mathbf{x0}$, $\mathbf{y0}$, $\mathbf{z0}$) cannot be on the boundary of any zone. To avoid a point source on a boundary move the source slightly (1.0e-08 cm) off the boundary and into a real interior zone. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 32**.

$$s1g$$
 nz $[x0 y0 z0]$

A photon point source at (x0, y0, z0). The most probable zone that the source is located in is nz.

Restrictions: **x0**, **y0**, **z0** are optional input that default to 0, 0, 0 (the origin) if not input. The point (**x0**, **y0**, **z0**) cannot be on the boundary of any zone. To avoid a point source on a boundary move the source slightly (1.0e-08 cm) off the boundary and into a real interior zone. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 45**.

A neutron source uniformly distributed in a right circular cylindrical shell parallel to the z axis, with inner radius ri, and outer radius ro. The center of the base of the cylinder is at (x0, y0, z0) and its length along the z axis is zlen.

Restrictions: **z0**, **zlen**, **x0**, **y0** are option input that default to 0, 0, 0, 0. If **zlen** = 0, the source is an annular disk. To align the cylinder with the x or y axis use **sentl 30**. To define a source in an angular sector of a cylinder use **source15**. The reference axis for launching particles is the z axis; the reference axis can be changed using **sentl 32**.

A photon source uniformly distributed in a right circular cylindrical shell parallel to the z axis, with inner radius ri, and outer radius ro. The center of the base of the cylinder is at (x0, y0, z0) and its length along the z axis is zlen.

Restrictions: **z0**, **zlen**, **x0**, **y0** are option input that default to 0, 0, 0, 0. If **zlen** = 0, the source is an annular disk. To align the cylinder with the x or y axis use **sentl 43**. To define a source in an angular sector of a cylinder use $\mathbf{s15g}$. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 45**.

source3 nz ri ro [z0 x0 y0 a1 a2 dcx dcy dcz b1 b2]

A neutron source uniformly distributed over a segment of a spherical shell with inner radius **ri** and output radius **ro**, centered at the point (**x0**, **y0**, **z0**). The segment extends between the angles **a1** and **a2** (degrees) from the axis of symmetry defined by **dcx**, **dcy**, **dcz**. When the axis of symmetry is the **z** axis, an angular section may also be specified between the angles **b1** and **b2**, which is measured clockwise from the y axis toward the x axis.

Restrictions: **z0**, **x0**, **y0** are option input that default to 0, 0, 0 (the origin). **a1**, **a2** are optional input that default to 180, 0 degrees. **dcx**, **dcy**, **dcz** are optional input that default to 0, 0, 1 (the axis of symmetry is the z axis). **b1**, **b2** are optional input that default to 360, 0 degrees. **b1** and **b2** are used only if the axis of symmetry is the z axis. The reference axis for launching particles is the Z axis; the reference axis can be changed using an **axis** input line.

A photon source uniformly distributed over a segment of a spherical shell with inner radius **ri** and output radius **ro**, centered at the point (**x0**, **y0**, **z0**). The segment extends between the angles **a1** and **a2** (degrees) from the axis of symmetry defined by **dcx**, **dcy**, **dcz**. When the axis of symmetry is the **z** axis, an angular section may also be specified between the angles **b1** and **b2**, which is measured clockwise from the y axis toward the x axis.

Restrictions: **z0**, **x0**, **y0** are option input that default to 0, 0, 0 (the origin). **a1**, **a2** are optional input that default to 180, 0 degrees. **dcx**, **dcy**, **dcz** are optional input that default to 0, 0, 1 (the axis of symmetry is the z axis). **b1**, **b2** are optional input that default to 360, 0 degrees. **b1** and **b2** are used only if the axis of symmetry is the z axis. The reference axis for launching particles is the z axis; the reference axis can be changed using an **axisg** input line.

source4 nz r [z0 x0 y0 a1 a2 dcx dcy dcz b1 b2]

A neutron source uniformly distributed over a segment of a spherical surface of radius \mathbf{r} , centered at the point $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The segment extends between the angles $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the axis of symmetry defined by \mathbf{dcx} , \mathbf{dcy} , \mathbf{dcz} . When the axis of

symmetry is the z axis, an angular section may also be specified between the angles **b1** and **b2**, which is measured clockwise from the y axis toward the x axis.

Restrictions: **z0**, **x0**, **y0** are option input that default to 0, 0, 0 (the origin). **a1**, **a2** are optional input that default to 180, 0 degrees. **dcx**, **dcy**, **dcz** are optional input that default to 0, 0, 1 (the axis of symmetry is the z axis). **b1**, **b2** are optional input that default to 360, 0 degrees. **b1** and **b2** are used only if the axis of symmetry is the z axis. The reference axis for launching particles is the z axis; the reference axis can be changed using an **axis** input line.

s4g nz r [z0 x0 y0 a1 a2 dcx dcy dcz b1 b2]

A photon source uniformly distributed over a segment of a spherical surface of radius **r**, centered at the point (**x0**, **y0**, **z0**). The segment extends between the angles **a1** and **a2** (degrees) from the axis of symmetry defined by **dcx**, **dcy**, **dcz**. When the axis of symmetry is the z axis, an angular section may also be specified between the angles **b1** and **b2**, which is measured clockwise from the y axis toward the x axis.

Restrictions: **z0**, **x0**, **y0** are option input that default to 0, 0, 0 (the origin). **a1**, **a2** are optional input that default to 180, 0 degrees. **dcx**, **dcy**, **dcz** are optional input that default to 0, 0, 1 (the axis of symmetry is the z axis). **b1**, **b2** are optional input that default to 360, 0 degrees. **b1** and **b2** are used only if the axis of symmetry is the z axis. The reference axis for launching particles is the Z axis; the reference axis can be changed using an **axisg** input line.

source5 nz [z0 zlen x0 xlen y0 ylen]

A neutron source uniformly distributed over a rectangular parallelepiped aligned with the axes and bounding by the planes x0, x0 + xlen, y0, y0 + ylen, z0, z0 + zlen

Restrictions: **z0**, **zlen**, **x0**, **xlen**, **y0**, **ylen** are all optional input that default to 0. If any of the lengths are zero, the source region may become a plane, a line, or a point. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 32**.

s5g nz [z0 zlen x0 xlen y0 ylen]

A photon source uniformly distributed over a rectangular parallelepiped aligned with the axes and bounding by the planes x0, x0 + xlen, y0, y0 + ylen, z0, z0 + zlen

Restrictions: **z0**, **zlen**, **x0**, **xlen**, **y0**, **ylen** are all optional input that default to 0. If any of the lengths are zero, the source region may become a plane, a line, or a point. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 45**.

source6 nz x1 y1 z1 x2 y2 z2

A neutron point source at (x1, y1, z1). The reference axis for launching particles is the direction from the source point (x1, y1, z1), toward the point (x2, y2, z2).

Restrictions: (x1, y1, z1) cannot be the same point as (x2, y2, z2). The angular distribution about the reference axis may be specified either by sentl 6 and 7, anglsrce, or by maec. maec and either maee or maech input may be used with source6.

A photon point source at (x1, y1, z1). The reference axis for launching particles is the direction from the source point (x1, y1, z1), toward the point (x2, y2, z2).

Restrictions: (x1, y1, z1) cannot be the same point as (x2, y2, z2). The angular distribution about the reference axis may be specified either by sentl 41 and 42, anglsrg, or by maecg. maecg and either maeeg or maechg input may be used with source6.

A neutron source of multiple spherical shells, with each spherical shell defined by a separate **source9** input. The neutron source for each spherical shell has a relative number of neutrons \mathbf{w} and is uniformly distributed in a spherical shell of inner radius \mathbf{r} and outer radius \mathbf{r} 0, centered at $(\mathbf{x}0, \mathbf{y}0, \mathbf{z}0)$. The initial time when neutrons are launched is \mathbf{t} .

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0 (the origin). **t** is optional input that defaults to 0. The reference axis for launching particles is the Z axis; the reference axis can be changed using an **axis** input line. Each spherical shell is assigned an index, 1, 2, 3, etc.,, in the order of **source9** input, that can be used to reference a shell when using **s9or10e** input.

s9g nz w ri ro
$$[z0 x0 y0 t]$$

A photon source of multiple spherical shells, with each spherical shell defined by a separate $\mathbf{s9g}$ input. The photon source for each spherical shell has a relative number of photons \mathbf{w} and is uniformly distributed in a spherical shell of inner radius \mathbf{ri} and outer radius \mathbf{ro} , centered at $(\mathbf{x0}, \mathbf{v0}, \mathbf{z0})$. The initial time when photons are launched is \mathbf{t} .

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0 (the origin). **t** is optional input that defaults to 0. The reference axis for launching particles is the Z axis; the reference axis can be changed using an **axisg** input line. Each spherical shell is assigned an index, 1, 2, 3, etc.,, in the order of **s9g** input, that can be used to reference a shell when using **s9or10eg** input.

```
source10 nz w ri ro [z0 zlen x0 y0 t]
s10 nz w ri ro [z0 zlen x0 y0 t]
```

A neutron source of multiple cylindrical shells aligned with the z axis, with each cylindrical shell defined by a separate **source10** input. The neutron source for each cylindrical shell has a relative number of neutrons \mathbf{w} and is uniformly distributed in a cylindrical shell of inner radius \mathbf{ri} and outer radius \mathbf{ro} . One end of the cylinder is centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and the length of the cylinder is \mathbf{zlen} along the positive z axis. The initial time when neutrons are launched is \mathbf{t} .

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0 (the origin). **zlen** is option input that defaults to 0, in which case the source is an annular disk. **t** is optional input that defaults to 0. To align the cylinder with the x or y axis use **sentl 30**. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 32** input line. Each cylindrical shell is assigned an index, 1, 2, 3, etc.., in the order of **source10** input, that can be used to reference a shell when using **s9or10e** input.

s10g nz w ri ro [z0 zlen x0 y0 t]

A photon source of multiple cylindrical shells aligned with the z axis, with each cylindrical shell defined by a separate s10g input. The photon source for each cylindrical shell has a relative number of photons w and is uniformly distributed in a cylindrical shell of inner radius ri and outer radius ro. One end of the cylinder is centered at (x0, y0, z0), and the length of the cylinder is zlen along the positive z axis. The initial time when photons are launched is t.

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0 (the origin). **zlen** is option input that defaults to 0, in which case the source is an annular disk. **t** is optional input that defaults to 0. To Align the cylinder with the x or y axis use **sentl 43**. The reference axis for launching particles is the Z axis; the reference axis can be changed using **sentl 45** input line. Each cylindrical shell is assigned an index, 1, 2, 3, etc.., in the order of **s10g** input, that can be used to reference a shell when using **s9or10eg** input.

s11cone nz w z0 z1 z2 a1 [x0 y0]

A neutron source of relative strength \mathbf{w} , uniformly distributed over the surface of a right circular cone, with its axis parallel to the z axis. The vertex of the cone is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The surface of the cone is at an angle $\mathbf{a1}$ (degrees) from the z axis, and the cone extended along the z axis between $\mathbf{z1}$ and $\mathbf{z2}$.

Restrictions: Do not use for reactivity problems. **x0**, **y0** are optional input that default to 0,0. The angle **a1** MUST be greater than 0 and less than 90 degrees. Both **z1** and **z2** MUST be on the same side of **z0**. The neutrons will be launched inward, in a cosine distribution relative to the normal to the surface. The neutron source can be defined by any number **s11cone**, **s11cyl**, **s11dsk** and **s11sph** input lines.

s11coneg nz w z0 z1 z2 a1 [x0 y0]

A photon source of relative strength \mathbf{w} , uniformly distributed over the surface of a right circular cone, with its axis parallel to the z axis. The vertex of the cone is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The surface of the cone is at an angle $\mathbf{a1}$ (degrees) from the z axis, and the cone extended along the z axis between $\mathbf{z1}$ and $\mathbf{z2}$.

Restrictions: **x0**, **y0** are optional input that default to 0,0. The angle **a1** MUST be greater than 0 and less than 90 degrees. Both **z1** and **z2** MUST be on the same side of **z0**. The photons will be launched inward, in a cosine distribution relative to the normal to the surface. The photon source can be defined by any number of **s11coneg**, **s11cylg**, **s11dskg** and **s11sphg** input lines.

s11cyl nz w r [z0 zlen x0 y0]

A neutron source of relative strength \mathbf{w} , uniformly distributed over the surface of a right circular cylinder of radius \mathbf{r} , with its axis parallel to the z axis. The base of the cylinder is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$ and its length along the positive z axis is **zlen**.

Restrictions: Do not use for reactivity problems. **z0, x0, y0** are optional input that default to 0,0, 0. **zlen** is option input that defaults to 0, in which case the source is a circle. The neutrons will be launched inward, in a cosine distribution relative to the normal to the surface. The neutron source can be defined by any number of **s11cone, s11cyl, s11dsk** and **s11sph** input lines.

s11cylg nz w r [z0 zlen x0 y0]

A photon source of relative strength \mathbf{w} , uniformly distributed over the surface of a right circular cylinder of radius \mathbf{r} , with its axis parallel to the z axis. The base of the cylinder is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$ and its length along the positive z axis is **zlen**.

Restrictions: $\mathbf{z0}$, $\mathbf{x0}$, $\mathbf{y0}$ are optional input that default to 0,0, 0. \mathbf{zlen} is option input that defaults to 0, in which case the source is a circle. The photons will be launched inward, in a cosine distribution relative to the normal to the surface. The photon source can be defined by any number of $\mathbf{s11coneg}$, $\mathbf{s11cylg}$, $\mathbf{s11dskg}$ and $\mathbf{s11sphg}$ input lines.

s11dsknz w ri ro [z0 d x0 y0]

A neutron source of relative strength \mathbf{w} , uniformly distributed over the surface of an annulus of a circular disk of inner radius \mathbf{ri} and outer radius \mathbf{ro} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and perpendicular to the z axis at $\mathbf{z0}$.

Restrictions: Do not use for reactivity problems. **z0**, **x0**, **y0** are optional input that default to 0, 0, 0. **d** is option input that defaults to +1.0. The neutrons will be launched from the disk in a cosine distribution relative to the normal to the surface, in the +z direction if d = -1.0, or in the -z direction if d = +1.0 (note, this is not a misprint). The neutron source can be defined by any number of **s11cone**, **s11cyl**, **s11dsk** and **s11sph** input lines.

s11dskg nz w ri ro [z0 d x0 y0]

A photon source of relative strength \mathbf{w} , uniformly distributed over the surface of an annulus of a circular disk of inner radius \mathbf{ri} and outer radius \mathbf{ro} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and perpendicular to the z axis at $\mathbf{z0}$.

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0. **d** is option input that defaults to +1.0. The photons will be launched from the disk in a cosine distribution relative to the normal to the surface, in the +z direction if $\mathbf{d} = -1.0$, or in the -z direction if $\mathbf{d} = +1.0$ (note, this is not a misprint). The photon source can be defined by any number of **s11coneg**, **s11cylg**, **s11dskg** and **s11sphg** input lines.

s11sph nz w r [z0 x0 y0 a1 a2]

A neutron source of relative strength \mathbf{w} , uniformly distributed over a segment of the surface of a sphere of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The segment extends between the angles $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the positive \mathbf{z} axis.

Restrictions: Do not use for reactivity problems. **z0, x0, y0** are optional input that default to 0, 0, 0. **a1** and **a2** are option input that default to 180, 0 degrees. The neutrons will be launched inward, in a cosine distribution relative to the normal to the surface. The neutron source can be defined by any number of **s11cone, s11cyl, s11dsk** and **s11sph** input lines.

s11sphg nz w r [z0 x0 y0 a1 a2]

A photon source of relative strength \mathbf{w} , uniformly distributed over a segment of the surface of a sphere of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The segment extends between the angles $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the positive \mathbf{z} axis.

Restrictions: **z0**, **x0**, **y0** are optional input that default to 0, 0, 0. **a1** and **a2** are option input that default to 180, 0 degrees. The photons will be launched inward, in a cosine distribution relative to the normal to the surface. The photon source can be defined by any number of **s11coneg**, **s11cylg**, **s11dskg** and **s11sphg** input lines.

source12 filename

A neutron source read from a file, or series of files, written by a previous problem using tally type 12.

Restrictions: Do not use for reactivity problems. **filename** is up to four characters that defines a series of files of the form NABCD000, NABCD001, etc., where N indicates neutron and ABCD are the four character **filename**. This **filename** is identical to that defined by the user with **sentl 51** in the previous problem that wrote the files. If **sentl 51** was not used in the previous problem, the default **filename** will be "cord". **Warning** - If both **source12** and **s12g** are used in a problem **sentl 18** MUST be set to 1.0, to define the

relative neutron and photon strengths; otherwise the photon source will be ignored. **Warning** - If either **source12** or **s12g** files are being used, and tally type 12 is used in the problem to write files, the default filenames cannot be used for both input and output tally files; if they are used the output tally files will overwrite the input files. See **sentl 51**.

s12g filename

A photon source read from a file, or series of files, written by a previous problem using tally type 12.

Restrictions: **filename** is up to four characters that defines a series of files of the form GABCD000, GABCD001, etc., where G indicates gamma (i.e., photons) and ABCD are the four character **filename**. This **filename** is identical to that defined by the user with **sentl 51** in the previous problem that wrote the files. If **sentl 51** was not used in the previous problem, the default **filename** will be "cord". **Warning** - If both **source12** and **s12g** are used in a problem **sentl 18** MUST be set to 1.0, to define the relative neutron and photon strengths; otherwise the photon source will be ignored. **Warning** - If either **source12** or **s12g** files are being used, and tally type 12 is used in the problem to write files, the default filenames cannot be used for both input and output tally files; if they are used the output tally files will overwrite the input files. See **sentl 51**.

s12iso

This option is identical to **source12**, except that the direction cosines will be randomly sampled from an isotropic distribution.

source13 nz r [z0 x0 y0 a1 a2]

A neutron source uniformly distributed over a segment of a spherical surface of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The segment extends between $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the positive z axis.

Restrictions: Do not use in reactivity calculations. **x0**, **y0**, **z0** are optional input that default to 0, 0, 0. **a1** and **a2** are optional input that default to 180, 0 degrees (which corresponds to a complete sphere). The reference axis for the angular distribution of neutrons is the outward normal to the spherical surface. This source can be used with multiple angle-energy spectra defined by **maec** and **maee** or **maeeh** input. Each spectrum will be generated between two cosine limits, relative to the reference axis.

s13g nz r [z0 x0 y0 a1 a2]

A photon source uniformly distributed over a segment of a spherical surface of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The segment extends between $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the positive z axis.

Restrictions: **x0**, **y0**, **z0** are optional input that default to 0, 0, 0. **a1** and **a2** are optional input that default to 180, 0 degrees (which corresponds to a complete sphere). The reference axis for the angular distribution of photons is the outward normal to the spherical surface. This source can be used with multiple angle-energy spectra defined by **maecg** and **maeeg** or **maeehg** input. Each spectrum will be generated between two cosine limits, relative to the reference axis.

source15 nz ri ro z0 zlen a0 da [x0 y0] s15 nz ri ro z0 zlen a0 da [x0 y0]

A neutron source uniformly distributed in a sector of a right circular cylindrical shell parallel to the z axis, with inner radius \mathbf{ri} and outer radius \mathbf{ro} . The base of the cylinder is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and it is of length \mathbf{zlen} in the positive z direction. The sector is defined starting at an angle $\mathbf{a0}$ (degrees), in the x-y plane measured from the positive y axis toward the positive x axis. The width of the sector is defined by \mathbf{da} (degrees), which may be positive or negative.

Restrictions: **a0** and **da** default to 0, so that they MUST be specified by input. **x0** and **y0** are optional input that default to 0, 0. If zlen = 0, the source is on a sector of an annular disk. To align the cylinder with the x or y axis use sentl 30. To specify a source in a complete cylindrical shell use source2. The reference axis for launching neutrons is the z axis; this can be changed using sentl 32.

s15g nz ri ro z0 zlen a0 da [x0 y0]

A photon source uniformly distributed in a sector of a right circular cylindrical shell parallel to the z axis, with inner radius \mathbf{ri} and outer radius \mathbf{ro} . The base of the cylinder is at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and it is of length \mathbf{zlen} in the positive z direction. The sector is defined starting at an angle $\mathbf{a0}$ (degrees), in the x-y plane measured from the positive y axis toward the positive x axis. The width of the sector is defined by \mathbf{da} (degrees), which may be positive or negative.

Restrictions: **a0** and **da** default to 0, so that they MUST be specified by input. **x0** and **y0** are optional input that default to 0, 0. If zlen = 0, the source is on a sector of an annular disk. To align the cylinder with the x or y axis use sentl 43. To specify a source in a complete cylindrical shell use s2g. The reference axis for launching neutrons is the z axis; this can be changed using sentl 45.

source16 nz w r [z0 a1 da]

A neutron source consisting of up to 120 circular arcs, with each arc described by its own **source16** input. The source has a relative strength \mathbf{w} and is on an arc of a circle of radius \mathbf{r} , centered at the point $(x, y, z) = (0, 0, \mathbf{z0})$, in a plane perpendicular to the z axis. The arc is defined by the starting angle $\mathbf{a1}$ (degrees), measured in the xy plane from the positive y axis toward the positive x axis. The width of the arc is defined by \mathbf{da} , which may be positive or negative.

Restrictions: **z0** is optional input that defaults to 0, **a1** and **da** are optional input that default to 0, 360 degrees. To align the source with the x or y axis use **sentl 30**. The reference axis for launching neutrons is the z axis; this can be changed using **sentl 32**.

s16g nz w r [z0 a1 da]

A photon source consisting of up to 120 circular arcs, with each arc described by its own $\mathbf{s16g}$ input. The source has a relative strength \mathbf{w} and is on an arc of a circle of radius \mathbf{r} , centered at the point $(x, y, z) = (0, 0, \mathbf{z0})$, in a plane perpendicular to the z axis. The arc is defined by the starting angle $\mathbf{a1}$ (degrees), measured in the xy plane from the positive y axis toward the positive x axis. The width of the arc is defined by \mathbf{da} , which may be positive or negative.

Restrictions: **z0** is optional input that defaults to 0, **a1** and **da** are optional input that default to 0, 360 degrees. To align the source with the x or y axis use **sentl 30**. The reference axis for launching photons is the z axis; this can be changed using **sentl 32**.

source17 nz r z0 x0 y0 kd

A neutron source uniformly distributed on the surface of a sphere of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The reference axis for launching neutrons will be the normal to the surface. The distribution of launch directions about the reference axis is defined by \mathbf{kd} , as follows,

kd

- 1 isotropic outward
- 2 isotropic inward
- 3 cosine distribution outward
- 4 cosine distribution inward

Restrictions: **kd** MUST be specified, therefore all other parameters that precede it in the input order MUST be specified.

s17g nz r z0 x0 y0 kd

A photon source uniformly distributed on the surface of a sphere of radius \mathbf{r} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The reference axis for launching photons will be the normal to the surface. The distribution of launch directions about the reference axis is defined by \mathbf{kd} , as follows,

kd

- 1 isotropic outward
- 2 isotropic inward
- 3 cosine distribution outward
- 4 cosine distribution outward

Restrictions: **kd** MUST be specified, therefore all other parameters that precede it in the input order MUST be specified.

Sentinels

TART95 uses sentinels to define many program options. All of the sentinels are listed together here. In addition, individual sentinels have been referenced in the sections to which they apply.

Sentinels are defined by using the TART95 keyword **sentl** followed by a pair of parameters: first a sentinel number and then a sentinel value. In the following each sentinel will be defined in numeral order. The number in parenthesis following the definition is the default value, i.e., if you do not specify this sentinel option by input, by default this is its value. It is important for users to be aware of these default values, i.e., if you do not specify the following options by input, then by default these values are still being used in your calculation, so you had better be aware of what you are using.

sentl 1 (0)

Type of particles to track. This defines both the types of sources (neutrons and/or photons) and which particles to track (should neutron induced photons be tracked?).

- o neutrons and neutron induced photons
- 1 only neutrons
- 2 only photons
- 3 neutrons, neutron induced photons and a photon source

Restrictions: for criticality (reactivity) problems only neutrons are tracked; any **sentl 1** input is ignored. If neutron induced photons are not tracked their energy is deposited locally at the point where they are created.

sentl 2 (20)

The number of batches (samples) of particles to follow. After each batch of particles the code will output results. The total number of histories for any given run is controlled by sentl 2 and 3: the number of batches of particles and the number of particles per batch.

For source problems the code will always run the indicated number of batches. For criticality problems the code will run no more than the indicated number of batches; it may run less if the statistics of the problem indicate that the answer has settled to a reliable answer.

For criticality problems it is suggested that you use a much larger number of batches (200), to insure that the calculation really converges to a reliable answer. If the code runs all of the indicated number of batches before convergence it will print a warning message. The user should consider this to be a warning that the results may not be

reliable. In this case it is suggested that you re-run the calculation using many more batches (2000).

sentl 3 (5000)

The number of particles per batch (sample). The total number of histories for any given run is controlled by **sentl 2 and 3** the number of batches of particles times the number of particles per batch.

It is recommended that you not use a small number of particles per batch.

For source problems the final statistics will be based on the total number of histories run = the number of batches times the number of particles per batch. In this case each history will be run completely independently. At the end of each batch the code will print complete results, so that the output file will be very large if you run a large number of batches. A good compromise is to first decide the total number of particles that you want to run and then run about 10 batches, each batch being about 1/10-th of the total number of histories you want to run.

For criticality problems the number of completely independent histories run is defined by the number of histories per batch. The same histories are tracked generation after generation until the distribution settles into an equilibrium distribution (in space, energy and direction). You will find that the time to convergence is related to the number of batches run times the number of neutrons per batch. In this case you should not use a small number of histories per batch. If you do the statistics for any given batch will be extremely poor and the code will have to run many batches in order to converge. The result will be that you will not save much time, compared to running larger batches of particles, i.e., using larger batches, convergence will occur after running a smaller number of batches.

sentl 4 (0.0)

Neutron source energy. For photons use **sentl 17**.

Restrictions: The default value of 0.0 indicates a neutron induced fission neutron spectrum. This is used for monoenergetic sources. If a spectrum is input this option is ignored. The neutron source energy must be within the range of TART95 multigroups = 1.307e-09 to 20.0 MeV.

sentl 5 (3)

Neutron tally type. For photons use **sentl 33**.

Restrictions: The default value (3) is neutrons entering each zone. See also, **ltype**, **probm**, **probmy**, **units**, **sentl 35**, **sentl 36**.

sentl 6 (2.0)

The cosine interval of the neutron source angular distribution. For photons use **sentl 41**.

The range of the angular distribution of the neutron source is defined by **sentl 6 and 7**. The angular distribution relative to the z axis, extended from **sentl 7** to **sentl 7** plus **sentl 6**. With the default values for **sentl 6** and **7 of** 2.0 and -1.0 the distribution extends from a cosine of -1.0 to a cosine of +1.0 =an isotropic angular distribution. For a monodirectional source directed straight up the z axis, use **sentl 7 1.0** and **sentl 6 0.0**. See also, **anglsrce**, **sentl 32**.

Restrictions: The entire cosine range from **sentl 7** to **sentl 7** plus **sentl 6**, cannot extend outside the legal cosine range -1.0 to +1.0.

sentl 7 (-1.0)

The start of the range of the neutron source angular distribution. For photons use **sentl** 42.

The range of the angular distribution of the neutron source is defined by **sentl 6 and 7**. The angular distribution relative to the z axis, extended from **sentl 7** to **sentl 7** plus **sentl 6**. With the default values for **sentl 6** and **7 of** 2.0 and -1.0 the distribution extends from a cosine of -1.0 to a cosine of +1.0 = 10 an isotropic angular distribution. For a monodirectional source directed straight up the z axis, use **sentl 7 1.0** and **sentl 6 0.0**. See also, **anglsrce**, **sentl 32**.

Restrictions: The entire cosine range from **sentl 7** to **sentl 7** plus **sentl 6**, cannot extend outside the legal cosine range -1.0 to +1.0.

sentl 8 (2.53e-08)

Minimum neutron energy. For photons use **sentl 9**.

For a positive minimum neutron energy any neutron with an energy less than this will have its energy set equal to the minimum. For a negative minimum neutron energy any neutron with an energy less than this will be discarded. When the default option is used neutrons are returned to the minimum energy.

When using thermal scattering, **sentl 39**, this option should be set to the minimum energy of the TART95 multigroup data = 1.307e-09. Failure to do so will prevent neutrons from fully thermalizing, e.g., for a room temperature problem and the default value of 2.53e-08, the neutrons cannot scatter to energies below the average Maxwellian energy of the target nuclei, so that they cannot fully thermalize.

Restrictions: The neutron source energy must be within the range of the TART95 multigroups = 1.307e-09 to 20.0 MeV.

sentl 9 (-1.0e-04)

Minimum photon energy. For neutrons see **sentl 8**.

For a positive minimum photon energy any photon with an energy less than this will have its energy set equal to the minimum. For a negative minimum photon energy any photon with an energy less than this will be discarded. When the default option is used, photons are discarded.

Restrictions: The photon source energy must be within the range of the TART95 photon data = 1.0e-04 to 30.0 MeV.

sentl 10 (1.0e-06)

Geometric uncertainty; referred to as **FUDGE.** When advancing to a boundary this amount will be added to the distance to the boundary to move the particle off the boundary and into a new zone.

Restrictions: This option must be positive and should be small compared to the dimensions, cm, of any zone in a problem. If this option is larger than the dimensions of a zone in a problem advancing particles by this amount can cause them to move completely across the zone and never "see" the zone. For most applications the default value is adequate; only if you are dealing with either extremely small or extremely large systems should you define a different value for this option.

sentl 11 (blank)

The filename of a file in which special input and output data is stored. See "sentl 11 Data File Contents".

Restrictions: The filename cannot exceed 8 characters; if it does, it will be truncated to 8 characters. The contents of the TART95 files differs from the contents of the standard TARTNP files. Contact the author for a copy of the FORTRAN routines required to read the TART95 files.

sentl 12 (0)

Initial random number seed sentinel.

0

This is the default is no sentl 12 is used; this means always use the same initial random number seed. This option should be used for most runs. With this option if you run the same problem more than once, you will always get exactly the same answer. **Warning** - you should never try to use this option (0) to run the same problem more than once to improve statistics. If you do, you will merely be running exactly the same histories over

again and get exactly the same - exactly correlated - results, which will not improve the accuracy of your results.

Otherwise

The entered value will be used as the initial random number seed. This option should only be used to continue calculations to run more histories to improve the statistics of the results. In this case you should always enter the random number seed printed by the code at the end of the run you wish to continue.

Restrictions: **Warning** - Using this option in any way other than described above is very dangerous. Entering anything except a legal random number seed printed by the code at the end of a previous run can produce unpredictable and unreliable results.

Warning - the definition of this option as used by TART95 differs from the definition used by the production version of TARTNP. TARTNP does not allow users to enter an initial random number seed to continue calculations. As used by TARTNP the input,

```
sentl 12 jr
```

Starting with TART97 the code now has 2,510 sequences, one trillion (10^{12}) samples apart. Input 0 (the default) to 2509 will use the selected sequence. Any other input is a fatal ERROR.

The older definition of this sentinel is as follows.

is interpreted based on the value to jr to mean,

```
< 1 \text{ or} = 6
```

Always use the same initial random number seed (the equivalent of inputting 0 for TART95; this is the default option for both TARTNP and TART95).

1 through 5

Use one of five built-in initial random number seeds. In octal these initial seeds are,

- 1 = 00647665707
- 2 = 02367441525
- 3 = 04107215343
- 4 = 05626771161
- 5 = 07346544777

> 6

Use a random initial random number seed.

sentl 13 (2.53e-08)

Minimum energy for editing the coordinates of neutrons entering a zone when using tally type 11 or 12. For photons see **sentl 14**.

Restrictions: The energy must be within the range of the TART95 multigroups = 1.307e-09 to 20.0 MeV. When using thermal scattering, **sentl 39**, this option should be set to the minimum energy of the TART95 multigroup data = 1.307e-09. Failure to do so will prevent neutrons with energies below 2.53e-08 MeV from contributing to tallies.

sentl 14 (1.0e-04)

Minimum energy for editing the coordinates of photons entering a zone when using tally type 11 or 12. For neutrons see **sentl 13**.

Restrictions: The energy must be within the range of the TART95 photon data = 1.0e-04 to 30.0 MeV.

sentl 15 (20.0)

Maximum energy for editing the coordinates of photons entering a zone when using tally type 11 or 12. For neutrons see **sentl 16**.

Restrictions: The energy must be within the range of the TART95 photon data = 1.0e-04 to 30.0 MeV. If your photon sources energies extend above 20 MeV (they can be up to 30 MeV), failure to increase this option to your maximum photon source energy will cause photons above 20 MeV not to contribute to tallies.

sentl 16 (20.0)

Maximum energy for editing the coordinates of neutrons entering a zone when using tally type 11 or 12. For photons see **sentl 15**.

Restrictions: The energy must be within the range of the TART95 multigroups = 1.307e-09 to 20.0 MeV.

sentl 17 (0.0)

Photon source energy. For neutrons see **sentl 4**.

Restrictions: The default value of 0.0 indicates a fission spectrum. This is used for monoenergetic sources. If a spectrum is input this option is ignored. The energy must be within the range of the TART95 photon data = 1.0e-04 to 30.0 MeV.

sentl 18 (0.0)

The number of source photons to follow per source neutron. This option is only used when **sentl 1** = 3 (track both neutron and independent photon sources) or when using both **source12** and **s12g**, where the neutron and photon source distributions are read from files.

Restrictions: when **sentl 1** = 3 this option defines the relative strength of the neutron and photon sources. In this case failure to define this option can cause photon sources to be ignored. For example if this option is 1.0, for each source neutron tracked, one source photon will be tracked. When using both **source12** and **s12g** this option **MUST** be set to 1.0, to insure that all source neutrons and photons, read from the files, are tracked.

sentl 19

Not used for older versions of tart. For tart98-3 and later versions the definition is,

sentl 19 (0)

Photon tally group sentinel. If 0, the default value, 50 photon tally groups will be used. If 1, there will be 175 photon tally groups. If 2, there will be 700 photon tally groups. See **cphotal** and **ltypeg**. For neutrons use **sentl 46**.

sentl 20 (0)

Multiband option. TART95 uses multigroup cross sections that do not include the effects of resonance self-shielded; so called, unshielded cross sections. Setting this option to 1 will cause the code to use the multiband method to account for the effects of resonance self-shielding.

Recommendation: The default value (0) has been kept for compatibility with TARTNP and any existing input parameter decks. But, it is highly recommended that you always turn on this option. Failure to do so can result in very unreliable results.

sentl 21 (20)

Number of batches (samples) for which short edits are output between each batch (sample) for which a long edit is output. A long edit is always output for the first and last batches (sample). Use -1 to get a long edit of every batch (sample). Use 0 or 1 to get a short edit every other batch (sample).

A short edit includes only a brief summary of balance or economy results summed over batches run so far, e.g., energy leaked, etc. A long edit include this brief summary plus all of the output requested by user input.

sentl 22 (0)

Mean free path edit sentinel. If 1, the code will not edit the mean free paths, cross section probabilities and energy deposition per collision.

sentl 23 (0)

Reaction edit sentinel. If 1, edits requested using the **reacted** option will not include reactions for each energy group; only the total for each reaction for each zone with be edited.

sentl 24 (0)

Next problem sentinel. If 1, input data for another problem follows the **end** input line for the current problem.

If you wish to run more than one problem this option **MUST** be set. Otherwise the code will terminate at the end of the current problem.

sentl 25 (0)

Fluorescence sentinel. If 1, photons produced by fluorescence will be tracked. Otherwise their energy will be deposited locally at the spatial point where they are created.

Recommendation: The default value (0) has been kept for compatibility with TARTNP and any existing input parameter decks. But, it is highly recommended that this option always be turned on that when tracking photons (either independent photon sources, or neutron induced photons).

sentl 26 (1)

Isotope reordering sentinel. If 2, for each material in the problem isotopes will be reordered in descending order by atomic abundance, to improve sampling efficiency.

Recommendation; It is recommended that when you define the materials for use in a problem, you define the order of isotopes in each material in descending order of importance. **sentl 26** can order isotopes based on atomic abundance, which is not necessarily the correct order by importance, since the cross sections for one isotope may be considerable larger or smaller than those of another isotope. You are in a much better position to decide what is or is not important in your problems, than this code is.

sentl 27 (32)

The number of neutron anisotropic scattering angular distribution intervals. The option values are 16, 8 or 4.

Recommendation: It is highly recommended that users never use this option. The tabulated neutron anisotropic scattering angular distributions in the neutron interaction data file (TARTNP) have been calculated to define 32 equally probable scattering cosine intervals that are sampled whenever a scattering event occurs. By changing from 32 to a smaller number of intervals all you will do is end up with a worse approximation to the original evaluated data.

sentl 28 (0)

Neutron energy-difference edit sentinel. For photons use **sentl 29**. If 1, the edits of each tally for each zone by energy and time will be repeated with each tally divided by the energy width of each tally group. If 2, the tallies will be multiplied by an input constant for each tally group, as specified on the **edif** input option. Note, if the **edif** input option is used, **sentl 28** will automatically be set to 2. This output will allow you to obtain energy dependent responses from the user supplied energy dependent table per MeV, as opposed to simply integrating over each energy tally bin.

Restriction: If this option is 2, you MUST use **edif** input. If using the **edif** input option, you need not set this option to 2, but you **MUST** not set it equally to any other value.

sentl 29 (0)

Photon energy-difference edit sentinel. For neutrons use **sentl 28**. If 1, the edits of each tally for each zone by energy and time will be repeated with each tally divided by the energy width of each tally group. If 2, the tallies will be multiplied by an input constant for each tally group, as specified on the **edifg** input option. Note, if the **edifg** input option is used, **sentl 29** will automatically be set to 2.

Restriction: If this option is 2, you MUST use **edifg** input. If using the **edifg** input option, you need not set this option to 2, but you **MUST** not set it equal to any other value.

sentl 30 (0)

Neutron source spatial coordinate transformation. For photons use **sentl 43**. When this option is used ALL source neutrons will have their initial spatial coordinates (X, Y, Z) switched are follows,

```
- (X, Y, Z) = No change
- (X, Z, Y) = Exchange Y and Z
- (Z, Y, X) = Exchange X and Z
- (X, -Z, Y) = Reverse the sign of Z, exchange Y and Z
- (-Z, Y, X) = Reverse the sign of Z, exchange X and Z
- (X, Y, -Z) = Reverse the sign of Z
```

Restrictions: Cannot be used for criticality problems, where the **critcalc** input option is used. **source3**, **source4** or **source9** will not be effected by this option if an **axis** input option is used.

sentl 31 (0.0)

Initial time coordinate of source neutrons.

sentl 32 (0)

Neutron source direction transformation. For photons use **sentl 45**. When this option is used ALL source neutrons will have their initial direction cosines (alpha, beta, gamma), switched are follows,

```
- (alpha, beta, gamma) = No change
- (beta,gamma,alpha) = Rotate left
- (gamma,alpha,beta) = Rotate right
- (beta,-gamma,alpha) = Reverse sign of gamma, rotate left
- (-gamma,alpha,beta) = Reverse sign of gamma, rotate right
- (alpha,beta,-gamma) = Reverse the sign of gamma
TART99 Update
- (-gamma,beta,alpha) = Rotation about y axis; use with sentl 30 4
```

Restrictions: **source3**, **source4** or **source9** will not be effected by this option if an **axis** input option is used.

sentl 33 (3)

Photon tally type. For neutrons use **sentl 5**.

Restrictions: The default value (3) is photons entering each zone. See also, **ltypeg**, **probm**, **probmv**, **units**, **sentl 35**, **sentl 36**.

```
sentl 34 (1.29 MeV)
```

Temperature of the source neutron induced neutron fission spectrum.

Restrictions: The temperature MUST be positive. Only used for source neutron induced neutron fission spectrum, i.e., sentl $\mathbf{4} = \mathbf{0.0}$. When this option is used the source neutron fission spectrum built into TART95 will be rescaled to have an average energy corresponding to the input value.

Recommendations: **Warning** - unless you are very familiar with fission spectra and understand the consequences of your action, it is highly recommended that you not use this option. There is no equivalent for source neutron induced photon fission spectrum.

sentl 35 (0)

Sentinel for additional edits.

1

An additional edit will be made for each problem multiplier specified on a **probm** or **probmv** input option, with the output multiplied by the problem multiplier.

2

The same as using option 1, but the output will be divided by the volume of each zone.

3

An additional edit will be made with the output multiplied by the zone multipliers specified on **units** (**zonemult**) input lines. An additional edit will be made for each problem multiplier, with the output multiplied by the problem multiplier and multiplier for each zone.

4

The same as using option 3, but the output will be divided by the volume of each zone.

5

The same as using option 3, but the output will be multiplied by the energy group multipliers specified on **edif** input lines, or divided by the energy width of each tally group, if **sentl** 28 = 1.

6

The same as using option 2, but the output will be divided by the mass of each zone, rather than the volume.

7

The same as using option 3, but the output will be divided by the mass of each zone, rather than the volume.

Restrictions: Depending on the option selected you may have to also input **probm** or **probmy, units** (**zonemult**) or **edif**. TART95 can only correctly calculate volumes, and therefore masses, for zones that are symmetric about the Z axis; in all other cases it arbitrary defines the volume of zones to be 1.0. Therefore in all other cases using this option to request output involving the volume and/or mass of zones will produce misleading results. Whenever you use this option please check the calculated volume for each zone, before relying on the accuracy of the results.

sentl **36** (0)

Sentinel for additional angular distribution edits, that are tallied by angle and energy for zones with tally types 7-10. The options are identical to those of **sentl 35**.

Restrictions: Same as for sentl 35.

sentl 37 (0)

Neutron cross section edit sentinel. If 1, output will include an edit of the neutron cross sections for each isotope in the problem by reaction type and energy.

sentl 38 (0)

Fission nu-bar sentinel. If 1, ALL fission nu-bar will be set to zero, so that no neutrons will be produced by fission.

If you have a final distribution of neutrons that already includes the effect of all fission neutrons produced you can use this option to transport them further and determine the effect that this distribution has.

sentl 39 (0)

Thermal scattering sentinel. If 1, thermal scattering will be used, otherwise all target nuclei will be assumed to be stationary.

The temperature of each zone should be defined by **emin** input; if not defined by input the default 2.53e-08 MeV (room temperature) will be used.

Restrictions: When this option is used the following options should also be used: **sentl 8 1.307e-08**, otherwise the code will use the default 2.53e-08 MeV and the neutrons will not be able to completely thermalize, **sentl 13 1.307e-08**, otherwise the code will use the default and not tally neutrons below 2.53e-08 MeV entering zones with tally type 11 and 12.

sentl 40

Not used.

sentl 41 (2.0)

The cosine interval of the photon source angular distribution. For neutrons use **sentl 6**.

The range of the angular distribution of the photon source is defined by **sentl 41** and **42**. The angular distribution relative to the z axis, extended from **sentl 42** to **sentl 42** plus **sentl 41**. With the default values for **sentl 41** and **42** of 2.0 and -1.0 the distribution extends from a cosine of -1.0 to a cosine of +1.0 =an isotropic angular distribution. For a monodirectional source directed straight up the z axis, use **sentl 42 1.0** and **sentl 41 0.0**. See also, **anglsrg, sentl 45**.

Restrictions: The entire cosine range from **sentl 42** to **sentl 42** plus **sentl 41**, cannot extend outside the legal cosine range -1.0 to +1.0.

sentl 42 (-1.0)

The start of the range of the photon source angular distribution. For neutrons use **sentl 7**.

The range of the angular distribution of the photon source is defined by **sentl 41** and **42**. The angular distribution relative to the z axis, extended from **sentl 42** to **sentl 42** plus **sentl 41**. With the default values for **sentl 41** and **42** of 2.0 and -1.0 the distribution

extends from a cosine of -1.0 to a cosine of +1.0 = an isotropic angular distribution. For a monodirectional source directed straight up the z axis, use **sentl 42 1.0** and **sentl 41 0.0**. See also, **anglsrg**, **sentl 45**.

Restrictions: The entire cosine range from **sentl 42** to **sentl 42** plus **sentl 41**, cannot extend outside the legal cosine range -1.0 to +1.0.

sentl 43 (0)

Photon source spatial coordinate transformation. For neutrons use **sentl 30**. When this option is used ALL source photons will have their initial spatial coordinates (X, Y, Z) switched are follows,

```
- (X, Y, Z) = No change
- (X, Z, Y) = Exchange Y and Z
- (Z, Y, X) = Exchange X and Z
- (X, -Z, Y) = Reverse the sign of Z, exchange Y and Z
- (-Z, Y, X) = Reverse the sign of Z, exchange X and Z
- (X, Y, -Z) = Reverse the sign of Z
```

Restrictions: s3g, s4g or s9g will not be effected by this option if an axisg input option is used.

sentl 44 (0.0)

Initial time coordinate for source photons. For neutrons use **sentl 31**.

sentl 45 (0)

Photon source direction transformation. For neutrons use **sentl 32**. When this option is used ALL source photons will have their initial direction cosines (alpha, beta, gamma), switched are follows,

```
- (alpha, beta, gamma) = No change
- (beta,gamma,alpha) = Rotate left
- (gamma,alpha,beta) = Rotate right
- (beta,-gamma,alpha) = Reverse sign of gamma, rotate left
- (-gamma,alpha,beta) = Reverse sign of gamma, rotate right
- (alpha,beta,-gamma) = Reverse the sign of gamma
TART99 Update
- (-gamma,beta,alpha) = Rotation about y axis; use with sentl 43 4
```

Restrictions: s3, s4g or s9g will not be effected by this option if an axisg input option is used.

sentl 46 (0)

Neutron tally group sentinel. If 0, the default value, 50 neutron tally groups will be used. If 1, there will be 175 neutron tally groups, without the necessity of requesting reaction edits (tally type 1). See **cneutal**, **reacted** and **ltype**. For photons use **sentl 19**.

sentl 47 (0)

Multiband edit sentinel (see **sentl 20**). If 0, standard edits (totals by reaction). If 1, extra tallies are edited: tritons produced per zone, (n,gamma) reactions by zone and isotope, and fission reactions by zone and isotope.

sentl 48 (55)

The size of the tally type 11 and 12 coordinate file will be changed to this option times 10,000 plus 20 words. See **sentl 51**.

sentl 49 (0)

Tally type energy group deletion sentinel.

If 1, no output by energy group, but output the totals and standard deviation of energy deposits, zone tallies and reactions, for each zone and time step.

If 2, the same as 1 without zone tallies.

If 3, the same as 1 with a standard full tally for the last sample. This option can be used to minimize output for intermediate batches and still allow you to obtain complete results at the end of the run. See **notal**.

sentl 50 (0)

(n,2n) tabular kinematics sentinel. If 1, use tabular kinematics for all (n,2n) reactions except for Be^9 (ZA = 4009).

sentl 51 ("cord")

Tally type 12 coordinate filename basis; an alphanumeric string of up to 4 characters. The filenames will be NABCD000 (neutrons) or GABCD000 (photons), where ABCD = the 4 characters input for this option.

Restriction: Use different filenames for **source12** or **s12g** input files and tally type 12 output, or the input files may be overwritten.

sentl 52 (0)

Relativistic kinematics sentinel. Not currently used.

sentl 53 (1.0e-08)

Geometric uncertainty (Fudge) used in defining zone volumes. This is no longer used by TART95; **sentl 10** is used for both volume calculation and advancing particles across boundaries.

Starting with TART98-1 sentl 53 is again used for Geometric uncertainty.

Neutron and Photon Edit and Tally (Output) types

Regardless of how fast and accurate a computer code is, its not very useful to you if you cannot obtain the output results that you want for your applications; this is the real proof of the pudding - can it solve your problem and give you the answers you want? One of the most powerful features of TART95 is the wide variety of tally and output options available to the user. To be able to take full advantage of the features of TART95 the user should be aware of what the standard TART95 default output includes and the availability of the following types of output options that you can specify by input.

Default Tally and Output

Generally output will be produced for every zone in a problem for each type of particle being tracked (neutrons and/or photons). The code will always output energy deposition for each zone. For all zones that contain material (all interior zones) particles will be tracked and both expected and analog deposition will be output. For all zones that do not contain material (exterior zones) the history will be terminated when the particle enters the zones and all of the particle's energy will be scored as deposition. In this case only the analog results will be output. This deposition will only be one integral number per zone, i.e., the results are not energy dependent.

If the user does not define what to score (tally) by default this is equivalent to specifying **ltype 3** (for neutrons) or **ltypeg 3** (for photons) which is particles entering each zone. These results are output both as a single integral number per zone as well as in energy dependent form using 50 tally groups for neutrons or photons. For details of the default 50 tally groups see tables 3 and 5 for neutrons and photons, respectively.

The user has the input option to change tally groups, but these cannot be arbitrarily specified. In all cases the boundaries of tally groups MUST be a subset of the 175 neutron group boundaries or photon energy points and MUST span the energy range of all particles in a problem. To change the tally groups for neutrons use **cneutal** and for photons use **cphotal**. These options can be used to specify up to 50 rew tally groups. For neutrons you can use 175 tally groups, rather than 50, using **sentl 46**, **reacted**, or **reactall**. There is no equivalent option for photons, so that the maximum output of photon tally bins is limited to 50.

Angular Distribution Tally and Output

Normally output will not include the angular distribution of particles. To obtain angular distributions use **ltype** (for neutrons) or **ltypeg** (for photons), equal to **7**, **8**, **9**, **10**. In this case you will obtain all other tallies requested PLUS this additional angular distribution output. However, in this case the neutron output is limited to 50 tally groups; you cannot obtain output in 175 tally groups. Angular distributions output will use 19 cosine bins; see table 8 for the cosine limits of these bins. To change the cosine bins use **cnang** (for neutrons) and **cpang** (for photons). For angular distributions the number of energy tally

groups will normally be decreased from 50 to 12; see table 8 for the energies of the 12 neutron and photon tally groups. For angular distribution output to change from the standard 12 groups use **angn** (for neutrons) and **angg** (for photon). When these options are used you can specify up to 24 energy tally bins, i.e., up to 25 tally limits.

Time Dependent Output

Normally if you do not specify anything by input the default is that all results are integrated over all time. As such the output from TART95 is NOT flux, it is fluence, which is flux integrated over all time. Similarly the energy deposition is the deposition integrated over all time. "All time" is defined as one second, 1.0e+8 shakes, which exceeds the half-life of a free neutron.

To obtain time dependent output use **centim** which applies to both neutrons and photons. When this option is used the output will be results integrated over the time intervals specified by the **centim** input.

WARNING - Once particles reach the maximum census time they are terminated. Therefore this is an effective means of limiting how long particles are followed. However, users MUST insure that the initial time of all source particles does not exceed the maximum census time of the problem. Otherwise, results may be inconsistent.

Response Functions

You can obtain additional output which is defined as the product of what you are tallying times an energy dependent response function. Use **edif** (for neutrons) and **edifg** (for photon). Results can be output in the form of either tally bin integrals (the default) or tally bin averages; for averages use **sentl 28** (for neutrons) and **sentl 29** (for photons).

This is a completely general means of modifying the output that you obtain. But the interpretation of the output up to the user and depends both on what you specify as the multiplier and what you specify as the scoring option. For example, if for neutrons you are scoring path length in each zone (**ltype 2**) and your **edif** input is a group averaged cross section the result will be the reactions (the product of cross section times fluence). You can use this option to calculate dose, a simple detector response, virtually anything that is proportional to what you are tallying. The only limit on the usefulness of this option is the imagination of the user.

The simplest use of this option is to merely change the units of your output. For example, normally the TART95 fluence (path length) output is in centimeters. If you would like output in any other units you can simply specify an energy independent multiplier.

Problem Multipliers

The response function capability described above is useful when you want to specify energy dependent multipliers for what you are tallying. The problem multiplier options

probm and **probmv** can be used to define a series of energy independent multipliers to obtain results for energy deposition and fissions per unit mass (**probm**) or volume (**probmv**). Used in conjunction with **sentl 35** and **36** the results can be specified to be either integral or average values.

The simplest use of this option is to merely change the units of your output; you can obtain output in as many different sets of options as you want. For example, normally the TART95 energy deposition output is in MeV. If you would like output in any other units you can simply specify an energy independent multiplier.

Zone Multipliers

The problem multipliers defined above are applied uniformly to all zones. If you would like to specify a multiplier for individual zones use the option **units** or **zonemult** (these are equivalent). These zone multipliers can be used in conjunction with the problem multipliers, described above. These zone multipliers apply to everything that you tally (not just energy deposition and fissions) and produces additional output listings, i.e., it does not replace the basic output, it supplements it.

Cross Section and Reaction Output

As a default you will always obtain output of the mean free path, probability of individual reactions (i.e., cross section ratio to the total) and expected energy deposition for each material used in a problem; not each evaluation, only each material, e.g., if you use hydrogen and oxygen to define water you will only obtain output of the total cross section for water. The mean free path and energy deposition are macroscopic quantities based on the total cross section and deposition as well as the density specified for each individual material.

If you would to obtain a listing of all cross sections for all 175 groups, reactions and isotopes used in a problem use **sentl 37**. **Warning** - for an average problem this option is not recommended, since it can result in a large amount of output.

If you would like output of the individual reactions that actually occur during the neutron Monte Carlo use **reacted** or **reactall**. **reacted** allows you to request for one zone the reaction with individual isotopes. You can use any number of **reacted** input lines to obtain output for as many isotopes in as many zones as you want. **reactall** allows you to request reactions for all isotopes in a list of zones. Anytime that you request **reacted** or **reactall** output the neutron tally groups will be changed from 50 to 175 groups and normally **reacted** and **reactall** output will be energy dependent by tally groups. If you would prefer only the total number of each reaction (integrated over tally groups) for each zone use **sentl 23**.

Additional and Non-Standard Tally and Output

You will always obtain a standard set of output results, as described above. You can modified what you tally and specify additional output results. An important point to understand is that if you request any additional output, it really is additional - it does not replace the basic output, that you will also receive.

In addition the user may specify additional types of output. The default option is in all cases 3 = the number of particles entering into each zone. This option may be changed zone by zone using **ltype** for neutrons or **ltypeg** for photons. For neutrons it may be changed globally using **sentl 5** for all zones that **ltype** is not specified, as it can using **sentl 33** for photons for all zones that **ltypeg** is not specified. This is a very powerful and versatile capability that the user should be aware of.

ltype l nz1 nz2 nz3....(3) ltype l nza thru nz2 (3)

Neutron edit type. **ltype** can be used to define the neutron edit type zone by zone; **sentl 5** allows it to be defined globally as the same value for all zones.

Restrictions: The default is 3 (particles entering the zone); see the complete list of choices, later in this report.

WARNING – when using ltype 11 or 12 to write binary files of neutron histories, be aware that the zone(s) that you wish to tally in MUST contain material; otherwise, when a particle enters an empty zone it is immediately absorbed, without allowing ltype 11 or 12 tally.

TART99 Update – Starting with TART99-4 ltype 11 or 12 can be used for empty zoines (zones to which no material is assigned); when a particle enters an empty zone, tally type 11 or 12 scores are checked for before absorbing the particle. This is a convenient option to use if you want to insure that each particle can result in at most one tally.

ltypeg 1 nz1 nz2 nz3....(3) ltypeg 1 nza thru nz2 (3)

Photon edit type. **ltypeg** can be used to define the neutron edit type zone by zone; **sentl 33** allows it to be defined globally as the same value for all zones.

Restrictions: The default is 3 (particles entering the zone); see the complete list of choices, later in this report.

WARNING – when using ltypeg 11 or 12 to write binary files of photon histories, be aware that the zone(s) that you wish to tally in MUST contain material; otherwise, when a particle enters an empty zone it is immediately absorbed, without allowing ltypeg 11 or 12 tally.

TART99 Update – Starting with TART99-4 ltypeg 11 or 12 can be used for empty zoines (zones to which no material is assigned); when a particle enters an empty zone, tally type 11 or 12 scores are checked for before absorbing the particle. This is a convenient option to use if you want to insure that each particle can result in at most one tally.

```
notal j nz1 nz2 nz3....(0)
notal j nz1 thru nz2 (0)
```

notal (no tally) can be used to indicate zones that should not be edited (no output). With the default value, 0, the zone will be edited by energy group and time. If 1, the zone will not be edited.

For example, in a problem that has 400 zones (numbered 1 through 400), if you only want output for zones 1, 2, 7, 10 and 100, the following input can be used,

```
notal 1 3 thru 400
notal 0 7 10 100
```

Note, the first line indicates no tallies for all zones except zones 1 and 2. The second line then indicates tallies for zones 7, 10 and 100.

Restrictions: The default is 0 = edit all zones. Setting **sentl 49 1** will give tallies only in zones where the **notal** option is 0, but setting **sentl 49 2** overrides **notal** and no zones will be edited by tally type.

The available types of tallies include,

- Expected collisions (MUST be used to get reaction edits)
- 2 Path length in centimeters
- 3 Number of particles entering a zone (DEFAULT). This is the only possible tally type for a void zone, e.g., the exterior,
 - non-re-entrant zone.
- 4 Energy transported into a zone
- 5 Flux entering a zone = number divided by cosine to normal
- 6 Energy flux entering a zone
- 7 Same as 3 with angular distribution
- 8 Same as 5 with angular distribution
- 9 Same as 4 with angular distribution
- Same as 6 with angular distribution
- 11 Writes a disk file
- 12 Writes a disk file
- Expected energy deposited by collision (photons only)
- Actual energy deposited by collision (photons only)
- Number of particles at census time (neutrons only)

- Write a disk file when entering a zone.
- Write a disk file after every collision in the zone.
- Collect particles that enter this zone, move them to a collector surface, and relaunch them, See **t1819**, **t18sph**, **t18dpl**.
- Collect particles that enter this zone, move them to a collector surface, and relaunch them in the +Z direction, See **t1819**.
- Number of Monte Carlo collisions
- 21 Number of photons that deposit energy in the zone (photons only).

Tally types 11 and 12 write disk files containing coordinates of particles entering the zone. Type 11 writes 4 coordinates $(X^2+Y^2, Z, \text{ velocity, and time})$, which can be used in (R, Z) symmetric systems. Type 12 writes 8 coordinates (X, Y, Z, alpha, beta, gamma, velocity, and time).

Tally type 16 writes the path length swept out in a zone, the time of entry, energy, zone number, batch number, and number of collisions. Tally type 17 writes the time of each collision and the energy lost in each collision.

Warning - any zone that you want tally type 11, 12, 16 or 17, binary output for **MUST** contain material. If it doesn't, the history will be terminated as soon as the particles enters the zone, before testing for any other type of tally.

Warning - the format of these binary files as used by TART95 differs from that used by the production version of TARTNP. For details of the contents of these files and FORTRAN routines that can be used to read them, contact the author.

Additional Output

In addition to the standard TART95 output the user may request additional output; almost anything can be scored and output.

```
edif j em(j) em(j+1) em(j+2)....
```

em(j), em(j+1), em(j+2).... are neutron tally type multipliers for tally energy groups j, j+1, j+2,..., respectively.

This option can be used to score and output anything that is proportional to the neutron tallies. For example, by inputting 50 cross sections (one for each of the standard 50 energy tally groups) for an activation reaction the results will be the activation due to this reaction. Similarly by inputting dose or damage data the results will be dose or damage. By inputting a simple detector response (simple in that it can only depend directly on the neutron energy), the output will be the detector response.

Restrictions: Using **edif** input automatically sets **sentl 28** to **2**, to indicate that the output will be multiplied by the **edif** multipliers for each neutron energy tally bin.

Example Input: The following input defines multipliers for the standard 50 neutron energy tally bins,

```
edif 1 4.0e-11 2.2e-11 8.0e-12 4.2e-12 2.3e-12 1.9e-12 edif 7 1.6e-12 1.3e-12 1.2e-12 1.1e-12 1.1e-12 1.1e-12 edif 13 1.2e-12 1.3e-12 1.7e-12 2.7e-12 4.4e-12 7.0e-12 edif 19 1.0e-11 1.4e-11 2.2e-11 3.1e-11 4.6e-11 6.4e-11 edif 25 8.0e-11 1.2e-10 1.7e-10 2.3e-10 3.2e-10 4.4e-10 edif 31 5.4e-10 6.0e-10 7.0e-10 9.2e-10 1.1e-09 1.3e-09 edif 37 1.5e-09 1.6e-09 1.8e-09 2.0e-09 2.3e-09 2.7e-09 edif 43 3.0e-09 3.3e-09 4.0e-09 4.1e-09 4.4e-09 5.0e-09 edif 49 6.0e-09 6.9e-09
```

edifg j em(j) em(j+1) em(j+2).....

em(j), em(j+1), em(j+2).... are photon tally type multipliers for tally energy groups j, j+1, j+2,..., respectively.

This option can be used to score and output anything that is proportional to the photon tallies. See **edif** above for a list of examples.

Restrictions: Using **edifg** input automatically sets **sentl 29** to **2**, to indicate that the output will be multiplied by the **edifg** multipliers for each photon energy tally bin.

Example Input: See **edif** above.

```
probm p1 p2 p3....
```

p1, p2, p3...are problem multipliers for energy deposited and fissions by zone and time step, in **MeV/gram**, for all zones. For each multiplier a separate output table will be produced.

Restrictions: Only one **probm** or **probmv** input line may be used in a problem, with up to 11 multipliers. **units** or **zonemult** (these two keywords are equivalent) may be used with **probm** or **probmv** to define multipliers by zone. For additional tally options using **probm** or **probmv**, see **sentl 35** and **36**, which allow additional scaling of output results by zone volume, energy tally group widths, etc..

Example Input: With the following input there will be three output tables, one without a multiplier, followed by a table using each of the two input multipliers.

```
probm 8.52e+4 48.56
```

probmv p1 p2 p3....

p1, p2, p3... are problem multipliers for energy deposited and fissions by zone and time step, in **MeV/cc**, for all zones. For each multiplier a separate output table will be produced.

Restrictions: Only one **probm** or **probmv** input line may be used in a problem, with up to 11 multipliers. **units** or **zonemult** (these two keywords are equivalent) may be used with **probm** or **probmv** to define multipliers by zone. For additional tally options using **probm** or **probmv**, see **sentl 35** and **36**, which allow additional scaling of output results by zone volume, energy tally group widths, etc..

Example Input: With the following input there will be three output tables, one without a multiplier, followed by a table using each of the two input multipliers.

probm 8.52e+4 48.56

reacted nz iza1 iza2.....

Requests additional edited output for zone **nz**, isotopes **iza1**, **iza2**,...(all isotopes if none are specified).

Restrictions: The tally type for zone **nz** MUST be **ltype 1** (expected collisions), **2** (path length) or **20** (Monte Carlo collisions); if not, its **ltype** will be set to **1**. If a **reacted** input line is used, the number of neutron tally groups is changed from 50 to 175. To suppress printing the entire array by energy, and to only print totals, set **sentl 23 1**.

Example Input: For zone 4 tally results of reactions with Li^6 (ZA = 3006),

reacted 4 3006

reactall nz1 thru nz2

Requests additional edited output for all isotopes in all zones from **nz1** through **nz2**, for which **ltype** has been set to **1**, **2** or **20** by the use of **ltype** input.

Restrictions: **ltype** input MUST be used to define the tally type by zone; it is NOT sufficient to use **sentl 5** to set the tally type to **1, 2** or **20**. To suppress printing the entire array by energy, and to only print totals, set **sentl 23 1**.

Example Input: For reaction edits for all isotope in zones 3 through 30, use the following input,

reactall 3 thru 30

units zm nz1 nz2 nz3.....(0.0) zonemult zm nz1 nz2 nz3.....(0.0) units zm nz1 thru nz2 (0.0)

zonemult zm nz1 thru nz2 (0.0)

zm is a multiplier for the indicated zones. This multiplier is used with **probm** and **probmv** to give additional output for the zone. To obtain output involving products of **units/zoneunit** and **probm** or **probmv** sentl 35 or 36 MUST be used to uniquely define the type of output requested.

Restrictions: The default is 0.0 = no additional output.

Changing Tally Bins

TART95 has standard options for tallying results as a function of energy and angle. The following options may be used to change these options, as well as to define time tally bins

angg - Change photon energy tally groups

angn - Change neutron energy tally groups

centim - Define time tally bins

cnang - Change neutron cosine tally bins

cpang - Change photon cosine tally bins

cneutal - Change neutron energy tally groupscphotal - Change photon energy tally groups

angg j i(j) i(j+1) i(j+2)......

The default photon tally groups for tally types 7 through 10 are re-defined. The new energy tally group \mathbf{j} has lower index $\mathbf{i}(\mathbf{j})$ and upper index $\mathbf{i}(\mathbf{j}+1)$, where $\mathbf{i}(\mathbf{j})$ and $\mathbf{i}(\mathbf{j}+1)$ refer to the standard 51 tally group energy boundaries.

Example Input: The following input replaces the standard 50 tally groups. The new tally group 1, is from standard tally group boundary 1 through 3, new tally group 2, is from standard tally group boundary 3 through 6, new 3 is from 6 through 9, etc.

```
angg 1 1 3 6 9 12 14 17 18 20 22 24 26 28 angg 14 29 30 31 34 36 37 38 40 42 45 47 51
```

Restrictions: No more than 25 tally group indices can be specified. Tally group energy boundaries MUST be in ascending energy order.

angn
$$j$$
 $i(j)$ $i(j+1)$ $i(j+2)$

The default neutron tally groups for tally types 7 through 10 are re-defined. The new energy tally group \mathbf{j} has lower index $\mathbf{i}(\mathbf{j})$ and upper index $\mathbf{i}(\mathbf{j}+1)$, where $\mathbf{i}(\mathbf{j})$ and $\mathbf{i}(\mathbf{j}+1)$ refer to the standard 51 tally group energy boundaries.

Example Input: The following input replaces the standard 50 tally groups. The new tally group 1, is from standard tally group boundary 1 through 3, new tally group 2, is from standard tally group boundary 3 through 6, new 3 is from 6 through 9, etc.

```
angg 1 1 3 6 9 12 14 17 18 20 22 24 26 28 angg 14 29 30 31 34 36 37 38 40 42 45 47 51
```

Restrictions: No more than 25 tally group indices can be specified. Tally group energy boundaries MUST be in ascending energy order.

```
centim t(1) t(2) t(3).....[&]
```

t(1), t(2), t(3)....are the times (in shakes) at which various output quantities in their respective time intervals will be accumulated and edited. If needed, end the line with the continuation symbol (&) and use additional lines without **centim** to define additional times. The default value is t(1) = 1.0e + 8 (accumulate results integrated over all time).

Example Input: To accumulate and output results between 0 and 5 microseconds (0 and 500 shakes) and 5 and 10 (500 and 1000 shakes), and 10 and 1000 microseconds (1000 and 100,000 shakes),

```
centim 500 1000 1.0e+5
```

WARNING - Once particles reach the maximum census time they are terminated. Therefore this is an effective means of limiting how long particles are followed. However, users MUST insure that the initial time of all source particles does not exceed the maximum census time of the problem. Otherwise, results may be inconsistent.

```
cnang j c(j) c(j+1) c(j+2).....
```

Change the default values of the cosine bins for neutron tally types 7 through 10. The new bin \mathbf{j} has limits $\mathbf{c}(\mathbf{j})$ and $\mathbf{c}(\mathbf{j}+1)$. The input values of \mathbf{c} will be rounded to the nearest 0.01. No more than 20 \mathbf{c} values (19 cosine bins) may be specified. The defined \mathbf{c} MUST span the entire cosine range -1.0 to +1.0.

Example Input: To use smaller bins for the forward (cosine near +1) and backwards (cosine near -1) range use the following input,

```
cnang 1 1.0 0.98 0.96 0.94 0.92 0.9 0.88 0.8 0.7 0.6 0.5 0 -0.03 cnang 14 -0.5 -0.8 -0.9 -0.94 -0.96 -0.98 -1.0
```

cpang j
$$c(j)$$
 $c(j+1)$ $c(j+2)$

Change the default values of the cosine bins for photon tally types 7 through 10. The new bin \mathbf{j} has limits $\mathbf{c}(\mathbf{j})$ and $\mathbf{c}(\mathbf{j+1})$. The input values of \mathbf{c} will be rounded to the nearest 0.01.

No more than 20 \mathbf{c} values (19 cosine bins) may be specified. The defined \mathbf{c} MUST span the entire cosine range -1.0 to +1.0.

Example Input: see **cnang** below.

```
cneutal j i(j) i(j+1) i(j+2)....
```

Defines neutron tally groups that differ from the standard 50 tally groups. The new energy tally group j has lower index i(j) and upper index i(j+1), where i(j) and i(j+1) refer to the standard 51 tally group energy boundaries. The final energy on the input line defines the upper limit of the last group of the line. i(1) MUST be 1. See **sentl 46**, **reactall**, **reacted**, **ltype**.

Example Input: The follow maps the 176 neutron multigroup energy bounds into a new tally group structure,

```
cneutal 1 1 3 5 12 16 19 21 23 26 32 38 41 46 55 67 74 81 84 cneutal 19 89 91 94 96 99 101 102 103 104 105 107 109 111 cneutal 32 112 113 114 117 119 121 123 124 125 126 128 132 cneutal 44 133 137 141 143 150 157 166 176
```

```
cphotal j i(j) i(j+1) i(j+2)....
```

Defines photon tally groups that differ from the standard 50 tally groups. The new energy tally group \mathbf{j} has lower index $\mathbf{i}(\mathbf{j})$ and upper index $\mathbf{i}(\mathbf{j}+1)$, where $\mathbf{i}(\mathbf{j})$ and $\mathbf{i}(\mathbf{j}+1)$ refer to the standard 51 tally group energy boundaries. The final energy on the input line defines the upper limit of the last group of the line. $\mathbf{i}(1)$ MUST be 1. See **ltypeg**.

Example Input: The follow maps the 176 photon energy bounds into a new tally group structure,

```
cphotal 1 1 3 5 12 16 19 21 23 26 32 38 41 46 55 67 74 81 84 cphotal 19 89 91 94 96 99 101 102 103 104 105 107 109 111 cphotal 32 112 113 114 117 119 121 123 124 125 126 128 132 cphotal 44 133 137 141 143 150 157 166 176
```

Monte Carlo Test Calculations

TART95 includes a number of options to check the geometry and statistically estimate the volume of zones, including,

```
    mcflood - Check for unassigned or overlapping spatial regions
    statistically estimate the volume of zones
```

mcvplane -

Checking for unassigned or overlapping spatial regions can now be done much more efficiently and effectively using the **TARTCHEK** interactive graphics code.

For spatial zones that are symmetric about the z axis TART95 can analytically calculate the volume of zones. Therefore **mcvdisk** and **mcvplane** need only be used for more general zones.

mcflood	frac	kgeom	p 1	l p 2	2 p3	p4	p5	p6	p 7
mcflood	frac	1	ri	ro	$\bar{z}0$	$\mathbf{x0}$	y 0	a1	a2]
mcflood	frac	2	ri	r0	z 0	zlen	[x0]	y 0]
mcflood	frac	3	x1	x2	y1	y 2	z1	$\mathbf{z}2$	

Check for unassigned or overlapping spatial regions in the volume defined by **kgeom** at an average sample density of **frac** per cc. Each point will be checked again all zones in a problem. If unassigned or overlapping space is found a message is printed. If 100 such cases are found the run will terminate.

If kgeom = 1, the volume is a segment of a spherical shell with inner radius ri, outer radius ro, centered at (x0, y0, z0), between angles a1 and a2 (degrees) from the z axis. x0, y0, z0 are optional input that default to 0, 0, 0. a1 and a2 are optional input that default to 180 and 0 degrees.

If **kgeom** = 2, the volume is a right circular cylindrical shell parallel to the z axis, with inner radius \mathbf{ri} , outer radius \mathbf{ro} , with one end of cylinder centered at ($\mathbf{x0}$, $\mathbf{y0}$, $\mathbf{z0}$), and length **zlen** along the positive z axis. $\mathbf{x0}$, $\mathbf{y0}$ are optional input that default to 0, 0.

If kgeom = 3, the volume is a rectangular parallelepiped aligned with the three major axes and bounded by planes at x1, x2, y1, y2, z1, z2.

Recommendation: This option is no longer recommended. To check geometry use the interactive graphics program **TARTCHEK** which includes many more checks than those considered by **mcflood**.

Example Input: For a sphere of radius 970.1 cm, centered at the origin, check the volume where z < 0 (180 to 90 degrees from the z axis), using a sampling density of 0.0001 samples per cc.

mcflood	0.0001 1 0.0 970.1 0 0	0 180.0 90.0
mcvdisk mcvdisk	frac ri ro w0 smax u0 v0 k frac ri ro z0 smax x0 y0	axis mzcheck nz 0 mzcheck nz
mcvdisk	frac ri ro x0 smax y0 z0	1 mzcheck nz
mcvdisk	frac ri ro y0 smax z0 x0	2 mzcheck nz

An alternate spelling for this keyword is **mcvdisc**. The volume of zones is estimated statistically by launching particles in a positive direction parallel to the \mathbf{w} axis (\mathbf{x}, \mathbf{y}) or \mathbf{z} ,

from an annulus of a circular disk with inner radius \mathbf{ri} and outer radius \mathbf{ro} , centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$, and perpendicular to the \mathbf{w} axis at $\mathbf{w0}$, to find the distance traversed in each zone. The particles will be randomly sampled at an average density \mathbf{frac} over the surface of the annulus, and will traverse a maximum distance of \mathbf{smax} , or until they reach a leakage zone. If $\mathbf{mzcheck} = \mathbf{1}$, the zone and space check option is turned on, and tests are made for overlapping zones at the launch point and each zone boundary crossing. The search over zones will begin with zone \mathbf{nz} , which may be 0 (default). Up to a combination of 27 $\mathbf{mcvdisk}$ and $\mathbf{mcvplane}$ input lines may be used. $\mathbf{Warning} - \mathbf{A}$ combination of a large \mathbf{frac} and $\mathbf{mzcheck}$ can be very time consuming.

Example Input: Use a disk perpendicular to the axis z (kaxis = 0) located at z1 = -7.0. The disk has an inner radius ri = 0.0 and an outer radius ro = 6.4 and is centered at x0 = 0, y0 = 0. Traverse a maximum distance smax = 8 Check zones and space (mzcheck = 1). Sample frac = 100 samples per unit area of the disk,

mcvdisk 100.0 0.0 6.4 -7.0 8.0 0.0 0.0 0 1

```
mcvplane frac u1 u2 v1 v2 w1 smax kaxis mzcheck nz
mcvplane frac x1 x2 y1 y2 z1 smax 0 mzcheck nz
mcvplane frac z1 z2 y1 y2 x1 smax 1 mzcheck nz
mcvplane frac x1 x2 z1 z2 y1 smax 2 mzcheck nz
```

The volume of zones is estimated statistically by launching particles in a positive direction parallel to the \mathbf{w} axis (\mathbf{x}, \mathbf{y}) or \mathbf{z} , from a rectangular area perpendicular to the \mathbf{w} axis at $\mathbf{w}\mathbf{l}$, and bounded by the limits $\mathbf{u}\mathbf{l}$ to $\mathbf{u}\mathbf{l}$ and $\mathbf{v}\mathbf{l}$ to $\mathbf{v}\mathbf{l}$, to find the distance traversed in each zone. The particles will be randomly sampled at an average density **frac** over the surface of the rectangle, and will traverse a maximum distance of **smax**, or until they reach a leakage zone. If $\mathbf{mzcheck} = \mathbf{l}$, the zone and space check option is turned on, and tests are made for overlapping zones at the launch point and each zone boundary crossing. The search over zones will begin with zone \mathbf{nz} , which may be 0 (default). Up to a combination of 27 $\mathbf{mcvdisk}$ and $\mathbf{mcvplane}$ input lines may be used. $\mathbf{Warning} - \mathbf{A}$ combination of a large \mathbf{frac} and $\mathbf{mzcheck}$ can be very time consuming.

Example Input: Use a plane perpendicular to the axis z (kaxis = 0) located at z1 = -7.0. The plane extend between x1 = -6.4 and x2 = 6.4, and y1 = -6.4 and y2 = 6.4. Traverse a maximum distance smax = 8. Check zones and space (mzcheck = 1). Sample frac = 100 samples per unit area of the rectangle,

mcvplane 100.0 -6.4 6.4 -6.4 6.4 -7.0 8.0 0 1

Collector Surfaces

Collector surfaces can be used to reposition and redirect particles. For example, consider a point isotropic source at the origin of our coordinate system and a small detector located a long distance away. If we track neutrons they will spread our over a spherical volume and the probability of a neutron actually reaching the detector can be very small.

By using a collector surface we can allow the neutrons to transport to a spherical surface with a radius slightly less than the radial distance to the detector. When the neutrons cross this spherical surface, if the zone that they enter defines a collector surface, we can reposition and redirect the neutrons toward the detector, thereby greatly increasing the probability of their actually reaching the detector.

Warning - Use collector surfaces with extreme care. Note, all particles entering a collector surface zone across any boundary are collected, and all particles are launched from only one side of the collector surface. Unless you carefully design your collector surface zones you can produce misleading results, that do not at all correspond to the situation you are trying to simulate.

It is imperative that collector plates ONLY be used in symmetric geometry, e.g., a simple spherical system, to avoid highly biasing results.

ltype (for neutrons) and **ltypeg** (for photons) tally 18 and 19 are used a collect particles entering a zone. You may collect particles in any number of zones in a problem. **t1819**, **t18sph** and **t18dpl** are used to define where to re-emit all collected particles. You may only use one set of **t1819**, **t18sph** and **t18dpl** in a problem.

t1819 nz r z0 n l1

If only **t1819** input used (no **t18sph** or **t18dpl** input) the collector surface is a circular disk perpendicular to the z axis, centered at the point $(0, 0, \mathbf{z0})$, with radius \mathbf{r} . All particles collected using **ltype** or **ltypeg** tally 18 or 19 are re-emitted in zone \mathbf{nz} . For tally type 18, they are then given a random direction, but with the same angle from the surface norm as before, except the z component of the direction is positive. For tally type 19, they are directed in the positive z direction (no x or y component). The collector surface area is $pi*\mathbf{r}^2$.

 ${f n}$ is a particle multiplier, i.e., for each particle collected ${f n}$ particles will be re-emitted. This will allow you to multiple otherwise small samples of particles. All zone numbers of ${f l}{f l}$ or greater will have their output re-normalized by $1/{f n}$ to return their results to the original source strength.

For a spherical segment collector surface use **t1819** and **t18sph** input; only allowed for tally type 18; see **t18sph**, below.

For a displaced spherical segment collector surface use **t1819** and **t18dpl** input; only allowed for tally type 18; see **t18dpl**, below.

Warning - Use this option with extreme care. Note, all particles entering any collector zone across any boundary are collected, and all particles are launched in zone **nz** from only one side of the collector surface.

Restrictions: the geometry must be spherically symmetric. Otherwise the rotation of particles to the collector is not valid.

t18sph [a1 a2 x0 y0]

The collector surface is a segment of a spherical surface. The sphere has a radius of \mathbf{r} , and is centered by $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0})$. The surface segment is centered at $(\mathbf{x0}, \mathbf{y0}, \mathbf{z0} + \mathbf{r})$, where \mathbf{r} and $\mathbf{z0}$ are defined by $\mathbf{t1819}$ input. The surface segment extends between the angles $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the positive \mathbf{z} axis, and measured from the center of the sphere. The collector surface area is $2*pi*[Cos(\mathbf{a2}) - Cos(\mathbf{a1})]*r^2$. All collected particles are remitted in zone \mathbf{nz} (\mathbf{nz} is defined by $\mathbf{t1819}$ input) at a random position on the collector surface. They are then given a random direction, but with the same angle from the surface as before, except that the component of the new direction in the radial direction of the spherical collector surface is positive.

Restrictions: **a1** and **a2** are optional input that default to 180 and 0 degrees, respectively. **x0** and **y0** are optional input that default to 0, 0. Note, the difference between **t18sph** which uses the radius **r**, on **t1819** input, and **t18dpl** which defines the radius based on (**x0**, **y0**, **z0**) and (**x1**, **y1**, **z1**). This option can only be used for tally type 18, and only for neutrons. **t1819** input is also required.

Warning - Use this option with extreme care. Note, all particles entering any collector zone across any boundary are collected, and all particles are launched in zone **nz** from only one side of the collector surface.

t18dpl a1 a2 x0 y0 x1 y1 z1

The collector surface is a segment of a spherical surface. The sphere has a radius of $\mathbf{r} = \mathbf{Sqrt}[(\mathbf{x1-x0})^2+(\mathbf{y1-y0})^2+(\mathbf{z1-z0})^2]$, and is centered by $(\mathbf{x1},\ \mathbf{y1},\ \mathbf{z1})$. The surface segment is centered at $(\mathbf{x0},\ \mathbf{y0},\ \mathbf{z0})$, where $\mathbf{z0}$ are defined by $\mathbf{t1819}$ input. The surface segment extends between the angles $\mathbf{a1}$ and $\mathbf{a2}$ (degrees) from the symmetry axis, which is from the center of the sphere to the center of the collector. The collector surface area is $2*pi*[Cos(\mathbf{a2}) - Cos(\mathbf{a1})]*r^2$. All collected particles are re-emitted in zone \mathbf{nz} (\mathbf{nz} is defined by $\mathbf{t1819}$ input) at a random position on the collector surface. They are then given a random direction, but with the same angle from the surface as before, except that the component of the new direction in the radial direction of the spherical collector surface is positive.

Restrictions: **a1** and **a2** are optional input that default to 180 and 0 degrees, respectively. **x0** and **y0** are optional input that default to 0, 0. Note, the difference between **t18sph** which uses the radius **r**, on **t1819** input, and **t18dpl** which defines the radius based on (**x0**, **y0**, **z0**) and (**x1**, **y1**, **z1**). This option can only be used for tally type 18, and only for neutrons. **t1819** input is also required.

Warning - Use this option with extreme care. Note, all particles entering any collector zone across any boundary are collected, and all particles are launched in zone **nz** from only one side of the collector surface.

TARTNP Keywords Not Currently used by TART95

The current version of TART95 does not have a restart capability. This means that the following TARTNP keywords cannot currently be used by TART95,

restart - Read a restart file to continue a calculation

fulltal - Read a restart file to perform a full edit

These options are described below, to document their former use, so that this information will not be lost from this newer TART95 documentation.

It is recommended that if you want to run more histories to improve statistics (the usual use of **restart**) you use the last random number seed printed at the end of your previous run, as input with **sentl 12** to run additional histories starting from exactly where the previous run ended. The results in the two (or more) output listing can then be added together to define your cumulative results.

restart file n

A previously run problem will be restarted from the restart file. If **n** is specified (any value), this input is treated a **fulltal** input (see, below). The complete problem input may consist of only **name**, **box**, **sentl 2**, **11**, **21** and **23** (only), **restart** (next to last line) and **end**. If **file** is omitted, the code will form the restart file name from the first 6 characters of the problem name on the **name** input line, which MUST be the same as for the original problem. When restarting a problem that was using tally type 11 or 12, the coordinate file that the code was filling when the previous run ended MUST be present. To **restart**, make a full edit, and then quit, see **fulltal**. Note, a restart file can only be used with exactly the same version of the code that created the restart file.

fulltal file

A previously run problem will be restarted from the restart file, a full edit will be made, and the run will then end. The complete input may consist of only **name**, **box**, **fulltal** and **end**. If **file** is omitted, the code will form the restart file name from the first 6 characters of the problem name on the **name** input line, which MUST be the same as for the original problem. Note, a restart file can only be used with exactly the same version of the code that created the restart file.

TARTNP Keywords Not Allowed by TART95

Every effort has been made to make TART95 input parameters and output listing look exactly like the standard production code TARTNP input and results. However, a few

TARTNP keywords have been judged to be very difficult to properly use and dangerous in the sense that they use can lead to erroneous and misleading results. Therefore the following TARTNP keywords are not allowed for use with TART95,

chegp - Use fewer than the standard 175 neutron groups
 xsec - Change neutron multigroup cross sections

xsecg - Change photon interaction cross sections

xsecount - Change neutron multigroup cross sections

These options are described below, merely to document their former use, so that this information will not be lost from this newer TART95 documentation.

chegp
$$j$$
 $i(j)$ $i(j+1)$ $i(j+2)$

Use fewer than the standard 175 neutron energy groups. The indices of the new groups j, j+1,... will be the original indices i(j), i(j+1),... The final i is the upper limit of the last group on the input line. The new set MUST include the original indices 1, 7, 25, 92, 114 and 176 (176 as the final i). If this option is used **cneutal** input MUST also be used to define neutron tally limits from the new (collapsed) neutron group structure.

This option to collapse groups has proven to be very dangerous to use and even the earlier TARTNP documentation recommended that it not be used.

xsec iso ireact j
$$s(j)$$
 $s(j+1)$ $s(j+2)$[&]

The group average neutron cross section for isotope **iso** (in the form ZZAAA) and reaction **ireact**, starting with energy group j, will be replaced by the values s(j), s(j+1),.... If needed, end the input line with the continuation indicator (&), and continuation another input line (with **xsec iso ireact j**) given more s values. See the table "Isotope Reaction Numbers" for a list of possible reactions. Note, this option does not apply when the Multiband option (**sentl 20**) is used.

This option to replace neutron multigroup cross sections has proven to be very dangerous to use. It is still included in TARTNP only for historical purposes, e.g., for compatibility with a few very old TARTNP input decks. These days if you want to change the cross sections it is easier to do while creating the TARTNP neutron interaction data file.

xsecg mat iso ir1 sm1 ir2 sm2 ir3 sm3

The photon interaction cross sections for material **mat**, isotope **iso** (in the form ZZAAA), and internal reaction numbers **ir1**, **ir2** and **ir3**, will be multiplied by **sm1**, **sm2** and **sm3**, respectively. The internal reaction number is: 1 for incoherent, 2 for coherent, 3 for pair production and 4 for photoelectric. No more than 19 **xsecg** input lines may be used.

This option to replace photon interaction cross sections has proven to be very dangerous to use. It is still included in TARTNP only for historical purposes, e.g., for compatibility

with a few very old TARTNP input decks. These days if you want to change the cross sections it is easier to do while creating the GAMDAT photon interaction data file.

xsecount iso icount j s(j) s(j+1) s(j+2)....[&]

The group average neutron cross section for isotope **iso** (in the form ZZAAA) and reaction count **icount**, starting with energy group j, will be replaced by the values s(j), s(j+1),.... If needed, end the input line with the continuation indicator (&), and continuation another input line (with **xsecount iso icount j** given more s values. See the table "Isotope Reaction Numbers" for a list of possible reactions. Note, this option does not apply when the Multiband option (**sentl 20**) is used.

This option to replace neutron multigroup cross sections has proven to be very dangerous to use. It is still included in TARTNP only for historical purposes, e.g., for compatibility with a few very old TARTNP input decks. These days if you want to change the cross sections it is easier to do while creating the TARTND neutron interaction data file

angg 99	ehist 47	reflq 37	source2 60
anglsrce 54	ehistg 48	reflx 37	source3 61
anglsrg 54	ellip2p 21	refly 37	source4 62
angn 100	ellipse 21	reflz 37	source5 63
axis 55	emin 41	restart 107	source6 63
axisg 55	eming 42	s10 64	source9 64
bjp 32	end 10	s10g 65	spher2p 20
blkbdy 46	enerangl 48	s11cone 65	spher2px 19
box 10	enranglg 48	s11coneg 66	spher2py 19
centim 100	espec 49	s11cyl 66	spher2pz 20
chegp 108	especg 49	s11cylg 66	sphere 18
cnang 100	eta 42	s11dsk 67	spherex 18
cneutal 101	fspec 50	s11dskg 67	spherey 18
cone 24	fspecg 50	s11sph 67	spherez 18
cone2p 27	fulltal 108	s11sphg 68	srotate 30
cone2px 26	genplane 17	s12g 69	surf 28
cone2py 27	gpl 17	s12iso 69	surfp 29
cone2pz 27	gpwgt 44	s13g 69	surfr 29
coner 26	jb 31	s15 70	t1819 105
conerx 25	ltype 94	s15g 70	t18dpl 106
conery 25	ltypeg 94	s16g 71	t18sph 106
conerz 26	maec 56	s17g 72	timdist 57
conex 23	maecg 56	s1g 60	timdistg 58
coney 24	maee 51	s2g 61	timspec 58
conez 24	maeeg 51	s3g 61	timspecg 58
cpang 101	maeeh 52	s4g 62	units 98
cphotal 101	maeehg 53	s5g 63	volume
critcalc 11	matl 38	s6g 63	weight 42
cyl 23	matlwp 39	s9 64	wgtgam 43
cylx 22	matz 40	s9g 64	xcone 23
cyly 22	mcflood 102	s9or10e 53	xplane 16
cylz 23	mcvdisk 103	s9or10eg 53	xsec 109
eangl 55	mcvplane 104	sentl 73	xsecg 109
eanglg 55	name 10	source1 60	xsecount 109
ebias 46	notal 94	source10 64	ycone 24
ebiasg 46	probm 97	source12 68	yplane 17
edif 96	probmy 97	source13 69	zcone 24
edifg 96	reactall 98	source15 70	zonejb 31
ediscr 47	reacted 98	source16 71	zonemult 98
ediscrg 47	reflgp 37	source17 71	zplane 1